Project No. 1744-22 October 31, 2024

ADDENDUM No. 3
to the
DRAWINGS AND PROJECT MANUAL
for
TARWATER VETERINARY CLINIC
802 E. CRINER ST.

MAGEE ARCHITECTS, L.P.
DESIGNERS • PLANNERS • INTERIORS

GRANDVIEW, TEXAS

PO Box 101445 Fort Worth, TX 76185 817.615.9558 voice 817.992.1877 cell magee-architects.com



3.01 GENERAL

- A. This addendum modifies the Permit Set of Drawings and Project Manuals, dated September 26, 2024, as noted within and shall become part of the contract documents.
- B. Bidders shall acknowledge receipt of this addendum as part of the written bid submitted. Failure to do so may subject bidder to disqualification.
- C. Each holder of bid documents registered with the Architect will receive a copy of the addendum. Each prime bidder is responsible for distribution of information conveyed by this addendum to its sub-bidders and suppliers.

3.02 REVISIONS TO SPECIFICATIONS

A. <u>SECTION 00 3132 GEOTECHNICAL DATA</u>:

Remove the previously issued Spec Section 00 3132 GEOTECHNICAL DATA in its entirety and ADD Section 00 3132 GEOTECHNICAL DATA (WITH GEOTECHNICAL REPORT) as attached & included as a part of this Addendum.

B. SECTION 07 4113 METAL ROOF, WALL & SOFFIT PANELS:

Remove the previously issued Spec Section 07 4113 METAL ROOF, WALL & SOFFIT PANELS in its entirety and ADD <u>Section 07 4113 METAL ROOF, WALL & SOFFIT PANELS</u> as attached & included as a part of this Addendum.

- C. <u>SECTION 09 6520 RESILIENT FLOORING LUXURY VINYL TILE</u> 2.01 Tile Flooring, Paragraph A., shall be revised to state the following:
 - A. Luxury Vinyl Tile: Printed film type, with transparent or translucent wear layer.
 - 1. Manufacturers:
 - a. Karndean, K-Trade Flooring; Luxury Flooring: www.ktradeflooring.com.
 - 2. Minimum Requirements: Comply with ASTM F1700, of Class III Type B.
 - 3. Wear Layer Thickness: 20 mil (0.50 mm).
 - 4. Total Thickness: 0.098 inch (2.5 mm).
 - 5. Color: Vivera PVP5151, 48" x 7", Gluedown

D. SECTION 09 6723 RESINOUS FLOORING:

ADD this Section in its entirety as Resinous Epoxy Flooring to be Added to the Project Scope. Location & Application is indicated on Revised Sheet SA03-A002, as attached & included as part of this Addendum.

- E. <u>SECTION 10 2600 WALL & DOOR PROTECTION</u> 2.02 Components, Paragraph A., shall be revised to Add Item #5 with the following requirement:
 - 5. Locations: Provide Stainless Steel Corner Guards at Outside Corners along circulation paths & high traffic areas.

F. SECTION 31 3213 CHEMICAL SOIL STABILIZATION:

ADD this Section in its entirety as Chemical Soil Stabilization is to be Added to the Project Scope, as attached & included as part of this Addendum.

NOTE: Chemical Injection Process is cited in Geotechnical Report on Page 17, Section 5.6.4 – Subgrade Improvements Using Chemical Injection.

3.03 REVISIONS TO DRAWINGS

A. **ARCHITECTURAL**

1. SP101 - ARCHITECTURAL SITE PLAN - DIMENSION CONTROL

Delete this sheet in its entirety & replace with the Revised Sheet SA03-SP101 as attached as a part of this addendum.

2. SP102 - SITE DETAILS

Delete this sheet in its entirety & replace with the Revised Sheet SA04-SP102 as attached as a part of this addendum

3. A002 - ROOM FINISH & DOOR SCHEDULE, TYPES

Delete this sheet in its entirety & replace with the Revised Sheet SA05-A002 as attached as a part of this addendum.

B. STRUCTURAL

1. S101 - FOUNDATION PLAN, SECTION & DETAILS

- A. Delete this sheet in its entirety & replace with the Revised Sheet SS101-S101 as attached as a part of this addendum.
- S301 FOUNDATION, SECTIONS & DETAILS Detail A6/301 Typical Pier Detail shall be revised to ADD the following clarification of drilling depth for piers:
 - A. Top of Grade Beam is at Elevation 674.90. The Bottom of the Slab (Top of Prepared Select Fill) is at Elevation 674.48. The depth of drilling is from the Elevation 674.48. The bearing of the pier is at 17 feet below this elevation. This Elevation of 657.48 may vary and will be verified by UES Testing Agency on Site Observation and Verification of each pier.

C. MECHANICAL

1. M002 - MECHANICAL SCHEDULES

A. Delete this sheet in its entirety & replace with the Revised Sheet SM01-M002 as attached as a part of this addendum.

2. M201 - MECHANICAL FLOOR PLAN

A. Delete this sheet in its entirety & replace with the Revised Sheet SM02-M201 as attached as a part of this addendum.

D. PLUMBING

1. P002 - PLUMBING SCHEDULES

A. Delete this sheet in its entirety & replace with the Revised Sheet SP01-P002 as attached as a part of this addendum.

E. ELECTRICAL

1. <u>E002 – ELECTRICAL DETAILS</u>

A. Delete this sheet in its entirety & replace with the Revised Sheet SE01-E002 as attached as a part of this addendum.

2. <u>E003 – ELECTRICAL PANELS, SCHEDULES</u>

A. Delete this sheet in its entirety & replace with the Revised Sheet SE02-E003 as attached as a part of this addendum.

3. E200 – ELECTRICAL SITE LAYOUT

A. Delete this sheet in its entirety & replace with the Revised Sheet SE03-E200 as attached as a part of this addendum.

4. <u>E201 – ELECTRICAL POWER FLOOR PLAN</u>

A. Delete this sheet in its entirety & replace with the Revised Sheet SE04-E201 as attached as a part of this addendum.

5. E202 - ELECTRICAL LIGHTING FLOOR PLAN

A. Delete this sheet in its entirety & replace with the Revised Sheet SE05-E202 as attached as a part of this addendum.

3.04 **ATTACHMENTS**

- A. Spec Section 00 3132 GEOTECHNICAL DATA (WITH GEOTECH REPORT)
- B. Spec Section 07 4113 METAL ROOF, WALL & SOFFIT PANELS
- C. Spec Section 09 6723 RESINOUS FLOORING
- D. Spec Section 31 3213 CHEMICAL SOIL STABILIZATION
- E. Sheet SA03-SP101 ARCHITECTURAL SITE PLAN DIMENSION CONTROL
- F. Sheet SA04-SP102 SITE DETAILS
 G. Sheet SA05-A002 ROOM FINISH & DOOR SCHEDULE, TYPES
- Sheet SM01-M002 MECHANICAL SCHEDULES
- Sheet SM02-M201 MECHANICAL FLOOR PLAN
- K. Sheet SP01-P002 PLUMBING SCHEDULES
- Sheet SE01-E002 ELECTRICAL DETAILS
- M. Sheet SE02-E003 ELECTRICAL PANELS, SCHEDULES
- N. Sheet SE03-E200 ELECTRICAL SITE LAYOUT
- O. Sheet SE04-E201 ELECTRICAL POWER FLOOR PLAN
- P. Sheet SE05-E202 ELECTRICAL LIGHTING FLOOR PLAN

END OF ADDENDUM No. 3

DOCUMENT 00 3132 GEOTECHNICAL DATA (WITH GEOTECH REPORT)

PART 1 GENERAL

1.01 DESCRIPTION

- A. Soil investigation report has been prepared by UES Professional Solutions 44, LLC, referred to hereinafter as the soils engineer.
- B. A copy of the complete report with log borings is bound herein.
- C. This report was obtained only for use by Architect/Engineer in design and is not a part of the contract documents.
- D. Report and log of borings are made available for Contractor's information, but are not a warranty of subsurface conditions.
- E. Additional Investigation: Contractor should visit the site and acquaint himself with the site conditions.

1.02 ROCK CLAUSE

- A. If material is so large, heavy or cumbersome that it cannot be removed with a John Deere 455 Loader-Backhoe, then that part of excavation that requires other methods of removal such as, but not limited to, pneumatic jack hammer, hydraulic rock breaker, or dynamite, will be billed on a time and material basis less the cost for removal by normal means.
- B. Some work done during the rainy season may cost more than summer time work. This should be clearly understood prior to commencement of work. Said projects may include but are not necessarily limited to, removing a roof over a finished space or soil excavation.
- C. Post hole excavation is typically accomplished with hand tools. In the event any obstructions are encountered, natural or otherwise, additional labor, equipment rental and/or materials required to remove the obstruction, such as but not limited to, jack hammer, two-man auger or drill rig, etc., may be billed on a time and materials basis or may incur increased costs.
- D. Drilling Due to the fact that the conditions below the surface cannot be seen, certain assumptions are made in order to provide an estimate of cost. What follows is a list of circumstances that may alter the cost and how it will be billed should such circumstances arise:
 - a. Obstruction time shall be charged for drilling time or delay time due to any sub-surface obstruction other than natural geological formation.
 - b. In the event that caving soils, sub-surface water, hard-rock, etc., conditions (drilling refusal) prohibits us from performing the job in a normal manner (using our rock auger equipment), the work will stop. Any additional work requested by the engineer beyond that point will be done pursuant to Change Order. Drilling refusal: less penetration than 1 inch in 5 minutes.
 - c. In the event that drilling refusal is encountered before assumed drill depth, the footage we are short times the deduct price shall be deducted from the contract price. Any additional drilling beyond that point, if required, will be done pursuant to Change Order.

END OF SECTION

GEOTECHNICAL ENGINEERING REPORT

GRANDVIEW TEXAS VETERINARIAN CLINIC

802 East Criner Street
Grandview, Texas
UES Project No. W242089-rev1
August 28, 2024

Prepared for:

MAGEE ARCHITECTS

P.O. Box 101445 Fort Worth, Texas, 76185 Attention: Mr. Alan Magee

Prepared by:





Environmental
Geotechnical Engineering
Materials Testing
Field Inspections & Code Compliance
Geophysical Technologies

August 28, 2024

Magee Architects

P.O. Box 101445 Fort Worth, Texas, 76185 Attention: Mr. Alan Magee

Re: Geotechnical Engineering Report

Grandview Texas Veterinarian Clinic

802 East Criner Street Grandview, Texas UES Project No. W242089-rev1

Dear Magee Architects:

UES Professional Solutions 44, LLC (hereinafter "UES") has performed a geotechnical exploration for the project referenced above. This study was authorized by Mr. Alan Magee on July 22, 2024 performed in accordance with UES Proposal No. 105652 dated July 1, 2024.

The purpose of this revision is to include the bearing capacity of drilled and underreamed piers bearing in shaly clay at a depth of about 17 ft below final grade.

This report contains results of field explorations and laboratory testing and an engineering interpretation of these with respect to available project characteristics. The results and analyses were used to develop geotechnical recommendations to aid in design of foundations and pavement.

UES appreciates the opportunity to be of service on this project. If we can be of further assistance, such as providing materials testing services during construction, please contact our office.

BRIAN J. HOY

August 28, 2024

Sincerely,

UES PROFESSIONAL SOLUTIONS 44, LLC

TBPE Firm No. 813

, per il e

Karina Cohuo Geotechnical Project Manager Brian J. Hoyt, P.E.

Area Managing Director

KC/BJH

TABLE OF CONTENTS

1.0	IN	TRODUCTION	1
2.0	FIE	ELD EXPLORATION	2
3.0	LA	BORATORY TESTING	3
4.0	SIT	TE CONDITIONS	3
4.1		General	3
4.2		Geology	4
4.3		Soil/Rock Conditions	4
4.4		Groundwater	5
5.0	ΑN	NALYSIS AND RECOMMENDATIONS	6
5.1		Seismic Site Classification	6
5.2		Potential Vertical Rise (PVR) of Expansive Soil	6
5.3		Construction Excavations	6
5.4		Groundwater Control	7
5.5		Earthwork	8
	5.5.1	Site Preparation	8
	5.5.2	Proofroll	8
	5.5.3	Construction Considerations	8
	5.5.4	Grading, Drainage, Other Considerations	9
	5.5.5	Fill	10
5.6		Foundation System	11
	5.6.1	Drilled and Underreamed Piers	12
	5.6.2	Slab Foundation (Alternative)	14
	5.6.3	Subgrade Improvement Using Moisture Conditioning	15
	5.6.4	Subgrade Improvement Using Chemical Injection	17
1	5.6.5	Floor Slabs used with Drilled and Underreamed Piers	18
	5.6.6	Structural Slab	18
5.7		Pavement	18
	5.7.1	Rigid Pavements	19
	5.7.2	Pavement Subgrade	20
6.0	LIN	MITATIONS/GENERAL COMMENTS	21

APPENDIX

Boring Location Plan – Figure 1 Logs of Borings Key to Soil Symbols and Classifications

1.0 INTRODUCTION

<u>Purpose and Scope</u>. The purpose of this geotechnical study was to evaluate some of the physical and engineering properties of subsurface materials at selected locations on the subject site to develop geotechnical engineering design parameters and recommendations for the proposed project. To accomplish this, the scope of this study included field exploration consisting of drilling test borings and collecting samples of the subsurface materials, performing laboratory testing on selected samples obtained during the field exploration, performing engineering analysis and evaluation of the subsurface conditions with respect to the project characteristics, and development of foundation and pavement recommendations suitable for the proposed project. The scope of services did not include an environmental assessment of the site.

<u>Project Description</u>. The project consists of a proposed single story commercial building with a plan area of less than 4,500 SF and pavement to include parking areas and driveways.

<u>Project Location</u>. The project is located at 802 East Criner Street in Grandview, Texas. A site plan illustrating the subject site is provided as Figure 1, the Boring Location Plan, in the Appendix.

<u>Site Grading Plan</u>. The site grading plan was not available at the time of writing this report. Our recommendations provided herein are on the basis that cuts and fills of up to 2 feet will be required to bring the site to grade. When the grading plans are available, we should be notified and allowed to review the site grading plan to assess and modify our recommendations, as necessary.

<u>Cautionary Statement Regarding Use of this Report</u>. As with any geotechnical engineering report, this report presents technical information and provides detailed technical recommendations for civil and structural engineering design and construction purposes. UES, by necessity, has assumed the user of this document possesses the technical acumen to understand and properly utilize the information and recommendations provided herein. UES strives to be clear in its presentation and, like the user, does not want potentially detrimental misinterpretation or misunderstanding of this report. Therefore, we encourage any user of this report with questions regarding its content to contact UES for clarification. Clarification will be provided verbally and/or issued by UES in the form of a report addendum, as appropriate.

<u>Report Specificity</u>. This report was prepared to meet the specific needs of the client for the specific project identified. Recommendations contained herein should not be applied to any other project on or off this site by the client or anyone else without the explicit approval of UES.

<u>This Report is NOT a Specification</u>. Recommendations in this report are not specifications. Geotechnical engineering requires significant experience and professional judgment. Conditions vary in the field which require and/or allow modification to recommendations provided herein at the discretion of the Geotechnical Engineer of Record.

2.0 FIELD EXPLORATION

<u>Test Borings</u>. The field exploration for this project included drilling a total of four (4) test borings. Two (2) test borings were drilled to a depth of about 25 ft and two (2) test borings were drilled to a depth of about 5 ft. The depth referenced in this report are measured from the existing ground surface at the respective boring location at the time of the field exploration.

UES determined the number and depth of the test borings and performed the boring operations. The boring locations were not surveyed. Rather, UES personnel located the borings in the field using a recreational hand-held GPS unit and therefore should be considered approximate. The approximate boring locations are provided in Figure 1, the Boring Location Plan, in the Appendix.

The test borings were advanced between sample intervals to the termination depth of the borings using a drilling rig equipped with a rotary head turning continuous flight augers.

Cohesive Soil Sampling. Cohesive soil samples were generally obtained using Shelby tube samplers in general accordance with American Society for Testing and Materials (ASTM) D1587. The Shelby tube sampler consists of a relatively thin-walled steel tube with a sharp cutting edge connected to a head equipped with a ball valve threaded for rod connection. The tube is pushed into the undisturbed soils by the hydraulic pulldown of the drilling rig. The soil specimens were extruded from the tube in the field, logged, tested for consistency using a hand penetrometer, sealed and packaged to maintain "in situ" moisture content. The consistency of cohesive soil samples was evaluated in the field using a calibrated hand penetrometer. In this test a 0.25-inch diameter piston is pushed into the undisturbed sample at a constant rate to a depth of 0.25-inch. The results of these tests are tabulated at the respective sample depths on the boring logs. When the capacity of the penetrometer is exceeded, the value is reported as 4.5+.

<u>Texas Cone Penetration (TCP)</u>. Texas Cone Penetration (TCP) test was used to assess the apparent in-place strength characteristics of the soil and rock type materials. In the TCP test procedure, a 3-inch outside diameter (OD) steel cone driven by a 170-pound hammer dropped 24 inches (340 ft-pounds of energy). The number of blows of the hammer required to provide 12 inches of penetration, or the inches of penetration of the cone due to 100 blows of the

hammer (whichever occurs first) are recorded on the field logs (reference: TxDOT, Bridge Design Manual).

<u>Groundwater Observations</u>. The test borings were performed using dry drilling techniques, which enabled the potential detection of groundwater during the drilling and sampling procedures and prior to backfilling and plugging the boreholes. Groundwater observations are shown in the Appendix – Boring Logs.

<u>Borehole Backfilling and Plugging</u>. Upon completion of the borings, the boreholes were backfilled with on-site soil cuttings.

3.0 LABORATORY TESTING

UES performs visual classification and any of a number of laboratory tests, as appropriate, to define pertinent engineering characteristics of the soils encountered. Laboratory tests are performed in general accordance with ASTM or other standards and the results included at the respective sample depths on the boring logs. Laboratory tests and procedures utilized during this geotechnical study are indicated in Table A.

TABLE A Laboratory Testing Performed								
Test Procedure Description								
ASTM D2166	Standard Test Method for Unconfined Compressive Strength of Cohesive Soil							
ASTM D2216	Standard Test Method for Laboratory Determination of Water (Moisture) Content of							
ASTIVI DZZIO	Soil and Rock by Mass							
ASTM D2487	Standard Classification of Soils for Engineering Purposes (Unified Soil Classification							
ASTIVI D2467	System)							
ASTM D4318	Standard Test Methods for Liquid Limit, Plastic Limit and Plasticity Index of Soils							
ASTM D4546	One Dimensional Free Swell Tests							

4.0 SITE CONDITIONS

4.1 General

<u>Current Conditions.</u> At the time of the field exploration, the site generally consisted of a vacant, grassy tract of land.

<u>Limitations</u>. Due to the intermittent nature and relatively low resolution of aerial photographs, as well as our lack of detailed information regarding the past land use of the site, our review should not be interpreted as eliminating the possibility of cuts and/or fills on site which could detrimentally affect future construction.

<u>Topography</u>. Cursory visual observation and review of topographical maps from public data available at <u>www.dfwmaps.com</u> indicates the site slopes down towards the northeast about 2 ft (Appx. Elev. 674 ft to Appx. Elev. 672 ft).

4.2 Geology

<u>Geologic Formation</u>. Based on geological atlas maps available from the Bureau of Economic Geology, published by the University of Texas at Austin, the project site lies within the Eagle Ford formation. The Eagle Ford formation is composed predominantly of shale with occasional platy beds of sandstone and limestone. Residual overburden soils associated with the Eagle ford Formation generally consist of clay soils with moderate to very high shrink/swell potential.

4.3 Soil/Rock Conditions

<u>Stratigraphy</u>. Descriptions of the various strata and their approximate depths and thickness in general accordance with the Unified Soil Classification System (USCS) are provided on the boring logs included in the Appendix. Terms and symbols used in the USCS are presented in the Appendix following the Boring Logs.

Subsurface conditions encountered in most of the borings generally consisted of clay, and/or shaly clay extending to the 25 ft or 5 ft termination depths of the borings. Subsurface conditions encountered in Boring 2 generally consisted of clay and shaly clay to a depth of about 24 ft below the ground surface underlain by shale extending to the 25 ft termination depth of the borings. Depths referenced in this report are measured from the existing ground surface at the respective boring location at time of the field exploration.

Depths provided on the boring logs are based on our Field Technician's and Engineer's interpretation of conditions believed to exist between actual samples retrieved. Therefore, depth information contains both factual and interpretive information. Lines delineating subsurface strata are approximate and the actual transition between strata may be gradual or not clearly defined. In addition, variations may occur between or beyond the boring locations.

4.4 Groundwater

<u>Groundwater Levels</u>. The test borings were advanced using continuous flight augers with intermittent sampling methods. These dry drilling techniques enable observation of potential groundwater seepage levels. Groundwater observations in the borings during this study are identified in Table B. Depths referenced in this report and in Table B below are measured from the existing ground surface at the respective boring location at time of the field exploration.

TABLE B									
Groundwater Conditions Depth Groundwater Initially Groundwater Depth Upon Complet									
Boring No.	Encountered (feet)	Drilling (feet)							
B-1	15	15							
B-2	Not Observed	Not Observed							
B-3	Not Observed	Not Observed							
B-4	Not Observed	Not Observed							

Long-term Groundwater Monitoring. The groundwater observations are indicative of the groundwater conditions present at the time the borings were drilled. The amount of water in an open borehole largely depends on the permeability of the soils encountered at the boring location. In relatively impervious soils, such as clayey soils, a suitable estimate of the groundwater depth may not be possible, even after several days of observation. Long-term monitoring of groundwater conditions via piezometers or groundwater monitoring wells was not performed during this study and was beyond the scope of this study. Long-term monitoring can reveal groundwater levels materially different than those encountered during measurements taken while drilling the borings.

<u>Groundwater Fluctuations</u>. The groundwater observations reported herewith are applicable to groundwater conditions at the time of drilling. Future construction activities may alter the surface and subsurface drainage characteristics of this site. Seasonal variations, temperature, land-use, proximity to water bodies, and recent rainfall conditions also influence the depth to the groundwater. With these considerations, UES recommends that the contractor verifies the groundwater elevation before construction starts.

5.0 ANALYSIS AND RECOMMENDATIONS

5.1 Seismic Site Classification

The Site Class assigned for seismic design considers various factors, such as the soil profile (whether it's soil or rock), shear wave velocity, and strength, averaged over a depth of 100 feet. As our borings didn't reach depths of 100 feet, we made determinations under the assumption that the subsurface materials beneath the borehole bottoms resembled those encountered at the termination depth. Following the guidelines outlined in Section 1613.3.2 of the 2018 International Building Code and Table 20.3-1 in the 2010 ASCE-7, we recommend utilizing Site Class C (very dense soil and soft rock) for seismic design purposes at this location.

UES Project No. W242089-rev1

July 23, 2024

5.2 Potential Vertical Rise (PVR) of Expansive Soil

Our findings indicate floor slabs constructed within 2 ft of existing grade could experience soil-related potential movements of about 5 inches due to shrinking and swelling of active clays.

Potential seasonal movements were estimated assuming fill material used to raise the grade will consist of onsite or similar material with a plasticity index of 45 or less. If the plasticity index of material used to raise the grade is higher than 45, potential movements could be higher than our estimates.

Potential seasonal movements were estimated in general accordance with methods outlined by Texas Department of Transportation (TxDOT) Test Method Tex-124-E, from results of absorption swell tests and engineering judgment and experience. Estimated movements were calculated assuming the moisture content of the in-situ soil within the normal zone of seasonal moisture content change varies between a "dry" condition and a "wet" condition as defined by Tex-124-E. Also, it was assumed a 1 psi surcharge load from the floor slab acts on the subgrade soils. Movements exceeding those predicted above could occur if positive drainage of surface water is not maintained or if soils are subject to an outside water source, such as leakage from a utility line or subsurface moisture migration from off-site locations.

5.3 Construction Excavations

<u>Short Term Excavations.</u> The contractor is responsible for designing any excavation slopes, temporary sheeting or shoring. Design of these structures should include any imposed surface surcharges. Construction site safety is the sole responsibility of the contractor, who shall also be

solely responsible for the means, methods and sequencing of construction operations. The contractor should also be aware that slope height, slope inclination or excavation depths (including utility trench excavations) should in no case exceed those specified in local, state and/or federal safety regulations, such as OSHA Health and Safety Standard for Excavations, 29 CFR Part 1926, or successor regulations. Stockpiles should be placed well away from the edge of the excavation and their heights should be controlled so they do not surcharge the sides of the excavation. Surface drainage should be carefully controlled to prevent flow of water over the slopes and/or into the excavations. Construction slopes should be closely observed for signs of mass movement, including tension cracks near the crest or bulging at the toe. If potential stability problems are observed, a geotechnical engineer should be contacted immediately. Shoring, bracing or underpinning required for the project (if any) should be designed by a professional engineer registered in the State of Texas.

5.4 Groundwater Control

Groundwater was encountered at a depth of about 15 ft below the ground surface in Boring 1. However, seasonal fluctuations and/or unforeseen environmental conditions may result in water being encountered at shallower depths. This groundwater could be encountered in excavations required for building pad preparation. We therefore recommend the Contractor provide a line item for dewatering in the bid package in case dewatering is required. Test pits should be performed prior to construction to verify groundwater conditions.

The Contractor is typically responsible for designing, installing and maintaining a dewatering system for groundwater control and taking precautions to avoid distress to nearby existing structures, as a result of dewatering. Dewatering systems should be designed, installed and monitored by personnel qualified and experienced with dewatering soils. We recommend the Contractor consider retaining a dewatering expert to assist in identifying, implementing and monitoring the most suitable and cost-effective method to control groundwater. The following is intended to provide guidance to the Contractor for dewatering systems.

In cohesive soils where seepage is usually low, groundwater is generally managed by collection in trench bottom sumps for pumped disposal. Care should be taken to have a redundant pumping system that allows for overnight pumping. Water must not be allowed to pond in the excavation bottoms. The softening of soils can lead to instability and caving of trench side walls.

Generally, the groundwater depth should be lowered to a depth of at least 3 ft below the planned excavation bottom to provide a firm working surface. Extended and/or extensive dewatering can result in settlement of existing structures in the vicinity; the Contractor is to take necessary precautions to monitor and minimize the effects on these structures.

5.5 Earthwork

5.5.1 Site Preparation

In the area of improvements, all concrete, trees, stumps, brush, debris, abandoned structures, roots, vegetation, rubbish and any other undesirable matter should be removed and properly disposed.

5.5.2 Proofroll

After completion of the necessary stripping, clearing, and excavating, and prior to placing any required fill, the exposed soil subgrade should be carefully evaluated by probing and testing. Any undesirable material (organic material, wet, soft, or loose soil) still in place should be removed.

The exposed soil subgrade should be further evaluated by proof-rolling with a heavy pneumatic-tired roller, loaded dump truck or similar equipment weighing approximately 20 tons to check for pockets of soft or loose material hidden beneath a thin crust of possibly better soil.

Proof-rolling procedures should be observed routinely by a Professional Engineer or their designated representative. Any undesirable material (organic material, wet, soft, or loose soil) exposed during proof-rolling should be removed and replaced with well-compacted material as outlined in Section 5.5.5. Prior to placement of any fill, the exposed soil subgrade should be scarified to a minimum depth of 6 inches and recompacted as outlined in Section 5.5.5.

5.5.3 Construction Considerations

<u>Surface Soils.</u> The soils encountered at and near the ground surface at this site are susceptible to changes in moisture. The presence of surface water due to precipitation, groundwater or other sources may result in a decreased ability to compact and work with the soil. It is common for these soils to pump when subjected to high levels of moisture. As such, construction difficulties should be anticipated, especially during the wet season or immediately after rain events.

Maintenance of Subgrade during Construction. Unstable conditions could arise during general construction activities, particularly if the soil is exposed to wet weather conditions and repetitive construction traffic. After grading is completed, it's crucial to maintain the moisture content of the subgrade before proceeding with pavement construction. Minimizing construction traffic over the finished subgrade is advisable. If the subgrade becomes frozen, desiccated, saturated, or disturbed, the affected material should either be removed or treated by scarification, moisture conditioning, and recompaction before pavement construction begins. UES should be retained to observe earthwork and to perform necessary tests and observations during subgrade preparation.

5.5.4 Grading, Drainage, Other Considerations

Efforts should be made to minimize the excessive wetting or drying of the underlying soil, as it can lead to swelling and shrinkage of these soil layers. Standard construction practices of providing good surface water drainage should be used. A positive slope of the ground away from any foundation should be provided. Ditches or swales should be provided to carry the run-off water both during and after construction. Stormwater runoff should be collected by gutters and downspouts and should discharge away from the buildings.

In areas with pavement or sidewalks adjacent to the structure, a positive seal must be maintained between the structure and the pavement or sidewalk to minimize seepage of water into the underlying supporting soils. Post-construction movement of pavement and flatwork is common. Normal maintenance should include examination of all joints in paving and sidewalks, etc. as well as re-sealing where necessary.

Since granular bedding backfill is used for most utility lines, the backfilled trench should not become a conduit and allow access for surface or subsurface water to travel toward the new structures. Concrete cut-off collars or clay plugs should be provided where utility lines cross building lines to prevent water from traveling in the trench backfill and entering beneath the structures.

Root systems from trees and shrubs can draw a substantial amount of water from the clay soils at this site, causing the clays to dry and shrink. This could cause settlement beneath grade-supported slabs such as floors, walks and paving. Trees and large bushes should be located a distance equal to at least one-half their anticipated mature height away from grade slabs. Lawn areas should be watered moderately, without allowing the clay soils to become too dry or too wet.

5.5.5 Fill

<u>Select Fill (Non-Expansive Fill)</u>. Select fill used as non-expansive fill should consist of soil with a liquid limit less than 35 and a Plasticity Index between 4 and 15. The select fill should be placed in loose lifts not exceeding 8-inches and should be compacted to at least 95 percent maximum dry density (per ASTM D-698) and at a moisture content between 1 percent below optimum and 3 percent above optimum moisture content. The subgrade to receive select fill should be scarified to a depth of 6 inches and compacted to 95 percent of the material's maximum standard Proctor dry density (ASTM D-698) at a workable moisture level at least 4 percentage points above optimum.

<u>Flexible Base Material (Non-Expansive Fill).</u> Flexible base material used as non-expansive fill for the building pad area should meet the requirements of TxDOT Item 247, Type A or D, Grade 1-2. The material should be compacted to a minimum 95 percent of standard Proctor maximum dry density (ASTM D 698) and within -2 to +3 percentage points of the material's optimum moisture content.

The following recommendations pertain to fill soils placed for general site grading as follows:

- Outside the designated building pad areas if moisture conditioning will be used as the method for subgrade improvement. Where moisture conditioning is used for subgrade improvement, all fill within the designated building pad areas and associated adjacent areas should meet the requirements of Section 5.6.3.
- For general grading including building areas below the select fill requirement if chemical injection as discussed in Section 5.6.4 will be used as the method for subgrade improvement.

<u>General Fill</u>. Clayey soils used for general fill with a plasticity index equal to or greater than 25 should be compacted to a dry density between 93 and 98 percent of standard Proctor maximum dry density (ASTM D 698). The compacted moisture content of the clays during placement should be within the range of +2 to +6 percentage points of the material's optimum moisture.

<u>General Fill</u>. Clayey soils with a plasticity index below 25 should be compacted to a dry density of at least 95 percent of standard Proctor maximum dry density (ASTM D 698) and within the range of 1 percentage point below to 3 percentage points above the material's optimum moisture content.

Clayey fill should be process and the largest particle or clod should be less than 6 inches prior to compaction.

<u>Fill Restrictions</u>. Non-expansive fill and general fill should consist of those materials meeting the requirements stated. Non-expansive fill and general fill should not contain material greater than 4 inches in any direction, debris, vegetation, waste material, environmentally contaminated material, or any other unsuitable material.

<u>Fill on Existing Slopes</u>. If fill is to be placed on existing slopes (natural or constructed) steeper than six horizontal to one vertical (6:1), the fill materials should be benched into the existing slopes in such a manner as to provide a minimum bench-key width of five (5) ft. This should provide a good contact between the existing soils and new fill materials, reduce potential sliding planes, and allow relatively horizontal lift placements.

<u>Cautionary Note</u>. It is extremely important that material placed within building pads be properly characterized using one or more representative proctor samples. The use of a proctor sample which does not adequately represent the select fill being placed can lead to erroneous compaction (moisture and density) results which can significantly increase the potential for swelling of the select fill. The plasticity index of select fill soils placed during construction should be checked every day to confirm conformance to the project requirements and consistency with the proctor being utilized.

5.6 Foundation System

<u>Appropriate Foundation Types</u>. The following foundation types are appropriate to the site based on the geotechnical conditions encountered:

- Drilled and Underreamed piers
- Slab foundation

<u>Foundation Determination</u>. Structural loading information was not provided for this study. We have assumed that structural loads will be typical for the type and size of building proposed. Recommendations for the foundation types are presented below. Final determination of the foundation type to be utilized for this project should be made by the Structural Engineer.

<u>Avoidance of Mixing Foundation Types</u>. Mixing of foundation types for a given building should be avoided. Where mixing of slab and drilled and underreamed piers is required for a given building, UES should be contacted to review the foundation plans prepared by the Structural

Engineer prior to construction. Slab foundations and drilled and underreamed pier foundations can have incompatible movement characteristics.

<u>Assumed Maximum Cut/Fill Depth</u>. The site grading plan was unavailable at the time of this study. Therefore, we have assumed that cut/fill of up to 2 feet will be required to bring the site to grade. In the event cut/fill in the building pad exceeds 2 feet, we should be notified and allowed to review the design to assess the suitability of the foundation recommendations provided. UES *must be allowed to review the finalized grading plan to assess the appropriateness of our recommendations*.

<u>Foundation Plans Review</u>. Our office should be contacted to review the foundation plans, details and related structural loads, prior to finalizing the design to check conformance with the recommendations presented herein.

5.6.1 Drilled and Underreamed Piers

<u>Applicability</u>. Drilled and underreamed pier foundations as described in this section are appropriate for the proposed structure. The drilled and underreamed piers should bear in shaly clay at least 17 ft below final grade.

Groundwater was encountered at a depth of about 15 ft below the ground surface in Boring 1. Some field adjustments in the depth of underreamed piers may be required in some areas to maintain the bottom of the piers above groundwater seepage. However, the depth of piers should also be sufficient to maintain the underream below the depth of moisture conditioned or chemically injected soils which are prone to caving. Adjustments in the depths of underreamed piers should be observed in the field by UES personnel. Test piers should be performed outside the building pad area, or between planned pier locations inside the building pad, just prior to construction to verify groundwater conditions and constructability of drilled piers. Provisions should be made for immediate placement of concrete.

<u>Bearing Capacity</u>. Drilled and underreamed piers bearing in shaly clay at least 17 ft below final grade can be dimensioned using a net allowable end-bearing pressure of 4.5 kips per sq ft and no skin friction component of resistance. The recommended bearing pressure contains a factor of safety of at least 3 considering a general bearing capacity failure.

<u>Uplift</u>. The uplift force on the piers due to swelling of the active clays can be approximated by assuming a uniform uplift pressure of 2.2 kips per sq ft acting over the perimeter of the shaft to a depth of 12 feet below final grade. The shafts should contain enough full-length reinforcing

steel to resist uplift forces. A reduced uplift adhesion of 1.0 kip per sq ft can be used over the portion of the pier shaft in contact with moisture conditioned or chemically injected soil. The uplift adhesion due to soil swell can be neglected over the portion of the shaft in contact with non-expansive fill material used in the building pad area.

Minimum Pier Spacing. The underreamed portion should be at least two (2) and not exceeding three (3) times the diameter of the shaft. The minimum clear spacing between edges of adjacent piers should be at least one (1) underream diameter, based on the larger underream.

<u>Settlement</u>. Elastic settlement of drilled piers constructed as described herein should be about 1 inch or less.

<u>Grade Beams.</u> All grade beams connecting piers should be formed and not cast in earthen trenches. Grade beams should be formed with a nominal 10-inch void at the bottom. Commercially available cardboard box forms (cartons) are made for this purpose. The cardboard cartons should extend the full length and width of the grade beams. Prior to concrete placement, the cartons should be inspected to verify they are firm, properly placed, and capable of supporting wet concrete. Some type of permanent soil retainer, such as pre-cast concrete panels, must be provided to prevent soils adjacent to grade beams from sloughing into the void space at the bottom of the grade beams. Additionally, backfill soils placed adjacent to grade beams must be compacted as outlined in Section 5.5.5 of this report.

<u>Construction Observation</u>. All foundation excavations should be properly monitored to verify loose, soft, or otherwise unsuitable material is removed. All foundation excavations should be monitored to verify foundations bear on suitable material. The bearing stratum exposed in the base of all foundation excavations should be protected against any detrimental change in conditions. Surface runoff water should be drained away from excavations and not allowed to collect. All concrete for foundations should be placed as soon as practical after the excavation is made. Piers should be excavated and concrete placed the same day. All pier shafts should be at least 1.5 ft in diameter for pier stability considerations, to facilitate clean-out of the base and for proper monitoring.

Prolonged exposure of the bearing surface to air or water will result in changes in strength and compressibility of the bearing stratum. Therefore, if delays occur, a new deeper penetration should be provided, in order to provide a fresh bearing surface.

The construction of all piers should be observed to verify compliance with design assumptions and to verify:

- 1. Observations during pier drilling should include, but not necessarily be limited to, the following items:
- 2. Verification of proper bearing strata and consistency of subsurface stratification with regard to boring logs,
- 3. Confirmation the minimum required penetration into the bearing strata is achieved,
- 4. Complete removal of cuttings from bottom of pier holes,
- 5. Proper handling of any observed water seepage and sloughing of subsurface materials,
- 6. No more than 2 inches of standing water should be permitted in the bottom of pier holes prior to placing concrete, and
- 7. Verification of pier diameter, underream size and steel reinforcement.

<u>Concrete Placement</u>. Concrete should be placed immediately after the excavation has been completed. In no event should a pier excavation be allowed to remain open for more than 8 hours. Concrete should have a slump of 5 to 7 inches and should not be allowed to strike the shaft sidewall or steel reinforcement during placement.

5.6.2 Slab Foundation (Alternative)

<u>General</u>. The proposed structure can be supported on a reinforced ground-supported slab foundation provided that recommendations in Sections 5.6.3 or 5.6.4— Subgrade Improvement are followed. The slab foundation should be conventionally reinforced or post-tension reinforced. The slab foundation should be designed with exterior and interior grade beams adequate to provide sufficient rigidity to the foundation system to sustain the vertical soil movements expected at this site as described above. All grade beams and floor slabs should be adequately reinforced with steel to minimize cracking as normal movements occur in the foundation soils.

<u>Bearing Capacity</u>. The slab bearing on a subgrade improved as discussed in Sections 5.6.3 or 5.6.4 can be designed using a net allowable bearing pressure of 1,500 psf. This bearing pressure is based on a safety factor of 3 against shear failure of the foundation bearing soils.

<u>Grade Beam Geometry</u>. Grade beams should bear at a minimum depth of 12 inches below final grade (supported on non-expansive fill material or moisture conditioned soils). The bottom of the beam trenches should be free of any loose or soft material prior to the placement of the concrete. Grade beams should have a minimum width of 10 inches to reduce the potential for localized shear failure.

<u>PTI Recommendations</u>. A slab constructed within 2 ft of existing grade will be subject to potential seasonal movements of about 5 inches based upon the information gathered during this study. Subgrade improvement as discussed in Sections 5.9.3 or 5.9.4 will be required to reduce potential movements to about 1 inch. The recommended foundation design parameters based on information published in the Post Tensioning Institute (PTI) Design of Post-Tensioned Slabs-on-

Ground, 3rd Edition, are summarized in Table C:

TABLE C									
Foundation Design Parameters per PTI 3 rd Edition									
Allowable PVR	Edge Moisture V	ariation Distance	Differential Soil Movement						
in Inches	(fe	eet)	(inches)						
	Center Lift	Center Lift Edge Lift		Edge Lift					
	8.5	4.0	1.2	1.0					

<u>Construction and Observation</u>. All foundation excavations should be properly monitored to verify loose, soft, or otherwise unsuitable material is removed. All foundation excavations should be monitored to verify foundations bear on suitable material. The bearing stratum exposed in the base of all foundation excavations should be protected against any detrimental change in conditions. Surface runoff water should be drained away from excavations and not allowed to collect. All concrete for foundations should be placed as soon as practical after the excavation is made. Prolonged exposure of the bearing surface to air or water will result in changes in strength and compressibility of the bearing stratum. Therefore, if delays occur, grade beam excavations for slab foundations should also be slightly deepened and cleaned.

To reduce cracking as normal movements occur in foundation soils, all grade beams and floor slabs should be adequately reinforced with steel. It is common to experience some minor cosmetic distress to structures with slab-on-grade foundation systems due to normal ground movements. A properly designed and constructed moisture barrier should be placed between the slab and subgrade soils to retard moisture migration through the slabs.

5.6.3 Subgrade Improvement Using Moisture Conditioning

<u>Subgrade Improvement Using Non-Expansive Fill and Moisture Conditioned Soil</u>. We understand it is desired to reduce the potential seasonal movement of the floor slab to about 1 inch. Movements could be reduced to about 1 inch by placing at least 2 ft of non-expansive fill between the bottom of the floor slab and top surface of moisture conditioned soil extending to a depth of 10 ft below the non-expansive fill material.

The moisture conditioned native clay soil should be compacted to 93 to 97 percent of the material's maximum standard Proctor dry density (ASTM D-698) at a workable moisture level at least 4 percentage points above optimum (with a higher limit of 7 percentage points) and placed in loose lifts not exceeding 8 inches. Soils with lower plasticity indices may need to compacted at moisture contents closer to optimum.

Subgrade improvement/moisture conditioning should extend at least 5 feet horizontally beyond the perimeter of the building and below any adjacent flatwork for which it is desired to reduce movements. The non-expansive fill should not extend beyond the building perimeter. Moisture conditioning should extend at least 10 ft beyond outward swinging doors and main entrances. If flatwork or paving is not planned adjacent to the structures (i.e. above the moisture-conditioned soils that extend beyond the building perimeter), a moisture barrier consisting of a minimum of 10-mil plastic sheeting with 8 to 12 inches of soil cover should be provided above the moisture conditioned soils.

The purpose of moisture-conditioning is to reduce the swell potential of the moisture-conditioned soil to 1 percent or less. Additional laboratory tests (i.e., standard Proctors, absorption swell tests, etc.) should be conducted during construction to verify the "target" moisture content for moisture-conditioning (estimated at 4 percentage points above the material's optimum moisture content as defined by ASTM D 698) is sufficient to reduce the swell potential of the processed soil to 1 percent or less. In addition, it is recommended samples of the moisture-conditioned material be routinely obtained during construction to verify the swell of the improved material is 1 percent or less.

Installation of moisture-conditioned soils should be monitored and tested on a full-time basis by a representative of UES to verify the soils tested were placed with the proper lift thickness, moisture content, and degree of compaction.

<u>Subgrade Improvement at Exterior Doorways</u>. Subgrade improvement should extend beneath sidewalk areas that abut exterior doorways to the building. Failure to perform subgrade improvement in these areas can increase the probability of differential heaving between exterior sidewalks and doorways, resulting in exterior doors that will not or have difficulty opening outward due to "sticking" caused by heaving sidewalk slabs. Sidewalks tied to pavements and other flatworks that extend beyond the subgrades treated for PVR reduction are subject to movements similar to those for untreated subgrades.

<u>Subgrade Moisture</u>. The slab subgrade is prone to drying after being exposed and should be kept moist prior to slab placement.

Movement Risk. Recommendations have been provided to mitigate the effects of soil movement. Some soil movement and related structural cracking and floor unevenness should be expected even after following recommendations in this report. The elimination of risk related to soil movement is typically not feasible. If some level of movement is not acceptable (about 1 inch) the floor slab should be structurally suspended above the ground surface on a drilled pier foundation system.

5.6.4 Subgrade Improvement Using Chemical Injection

As an alternative to moisture conditioning, movement of the floor slab could be reduced to about 1 inch by placing a minimum 2-ft cap of non-expansive material between the bottom of floor slab and the top surface of 10 ft of chemical injected soil. Non-expansive fill could consist of select fill or flexible base material as described in Section 5.5.5. The lateral extents of chemical injection, non-expansive fill and any required plastic sheeting should match that recommended for moisture conditioning in Section 5.6.3.

Chemical injection consists of injecting the clayey soils with a proprietary chemical specifically formulated for long-term reduction of shrink-swell capacity in expansive clayey soils. The Client should obtain appropriate documentation from the manufacturer indicating the chemical is environmentally safe and long lasting (effective for 10 years or more). All references should be obtained and verified. Chemical injection proposals should only be considered from contractors whose chemicals and processes have been studied and shown to be effective by a major U.S. research university.

Satisfactory completion of the injection process will have been achieved when the desired allowable percent free swell has been achieved in the injected soils. In order to reduce overall building pad movements to about 1 inch, the resulting measured free swell of the injected material should not exceed 1 percent. Multiple passes with chemical injection may be required to meet this design requirement. The performance of post-injection free swell testing by ALPHA should be employed as acceptance criteria in engineering analysis to examine accomplishment of the intended objectives of the injection treatment.

Construction specifications as related to the chemical injection process should be provided by the contractor due to the proprietary nature of the chemicals used during the injection process. This includes acceptance criteria and any warranty.

Maximum benefits of this procedure can best be achieved provided the entire process is carefully observed and monitored by UES.

5.6.5 Floor Slabs used with Drilled and Underreamed Piers

If some slab movement is tolerable (about 1 inch), the floor system of the building can consist of a concrete slab designed to bear uniformly on improved soils. Subgrade improvement to reduce potential for floor slab movements are provided in Sections 5.6.3 or 5.6.4. In choosing this method of floor slab movement reduction, the Owner is accepting some post construction seasonal movement of the floor slab (about 1 inch).

UES Project No. W242089-rev1

July 23, 2024

If a soil-supported floor slab is utilized for the planned buildings, consideration should be given to a "floating" (fully ground supported, and not structurally connected to walls or foundations) floor slab. This can reduce the risk of cracking and displacement of the floor slab due to differential movements between the slab and foundations. A floor slab doweled into perimeter grade beams can develop a plastic hinge (crack) parallel to and approximately 5 to 10 ft inside the building perimeter. Differential movements can still occur between the grade beam and a "floating" floor slab. The structural engineer should determine the need for connections between the slab and structural elements and determine if control joints to limit cracking are needed. A properly designed and constructed moisture barrier should be placed between the slab and subgrade soils to retard moisture migration through the slab.

<u>Moisture Barrier</u>. A moisture barrier should be used beneath the floor slab in areas where floor coverings will be utilized (such as, but not limited to, wood flooring, tile, linoleum, and carpeting).

5.6.6 Structural Slab

In view of the potential seasonal movements (about 5 inches as discussed in Section 5.2), the most positive floor system for the building supported on drilled piers is a slab suspended completely above the existing expansive soils. At least 12 inches of void space should be provided between the bottom of the floor slab, or lowest suspended fixture, and top surface of the underlying expansive clays. A ventilated crawl space is preferred. Provisions should be made for (a) adequate drainage of the under-floor space and (b) differential movement of utility lines, including areas where the utility penetrates through the grade beam and/or where the utility penetrates below grade areas.

5.7 Pavement

<u>General</u>. To permit correlation between information from test borings and actual subgrade conditions exposed during construction, a qualified Geotechnical Engineer should be retained to

provide subgrade monitoring and testing during construction. If there is any change in project criteria, the recommendations contained in this report should be reviewed by our office.

<u>Civil and Drainage Consideration</u>. Calculations used to determine the required pavement recommendations are based only on the physical and engineering properties of the materials used and conventional thickness determination procedures. Pavement joining buildings should be constructed with a curb and the joint between the building and curb should be sealed. Related civil design factors such as subgrade drainage, shoulder support, cross-sectional configurations, surface elevations, reinforcing steel, joint design and environmental factors will significantly affect the service life and must be included in preparation of the construction drawings and specifications, but all were not included in the scope of this study. Normal periodic maintenance will be required for all pavement to achieve the design life of the pavement system.

Please note, the recommended pavement sections provided below are considered the minimum necessary to provide satisfactory performance based on the expected traffic loading. In some cases, City minimum standards for pavement section construction may exceed those provided below.

5.7.1 Rigid Pavements

After subgrade improvement as recommended in Section 5.7.2, PCC (reinforced) pavement sections are recommended in Table D.

TABLE D									
Recommended PC	Recommended PCC Pavement Sections								
Paving Areas and/or Type	Subgrade Preparation	PCC Thickness,							
, , , , , , , , , , , , , , , , , , ,	and Thickness	Inches							
Parking Areas Subjected Exclusively to	6 inches of Scarified and	5							
Passenger Vehicle Traffic	Compacted Subgrade ¹	J							
Drive Lanes, Fire Lanes, Areas Subject to Light	6 inches Lime Stabilized	6							
Volume Truck Traffic	o inches Linie Stabilized	U							
Dumpster Traffic Areas, Areas subject to	6 inches Lime Stabilized	7							
Moderate Volume Truck Traffic	o inches Linie Stabilized	,							

¹ Lime stabilization of the pavement subgrade is recommended for drive lanes, fire lanes, and pavement subject to truck traffic (see Section 5.7.2). Lime treatment of the pavement subgrade is not required for pavements subjected exclusively to passenger vehicle traffic, although lime treatment is these areas would be generally beneficial to the long-term performance of the pavement.

<u>Concrete</u>, <u>Reinforcing</u> and <u>Jointing</u>. Portland-cement concrete should have a minimum compressive strength of 3,500 psi. Concrete should be designed with 4.5 + 1.5 percent entrained air. Joints in concrete paving should not exceed 15 ft. Reinforcing steel should consist of No. 3 bars placed at 18 inches on-center in two directions.

<u>Alternate Pavement Thickness</u>. Concrete pavement thicknesses provided above can be increased an extra 1 inch (corresponding reinforcing requirements must be changed) as a substitution for lime stabilization of the pavement subgrade. Prior to construction of pavement on untreated clay subgrade soil, the exposed subgrade should be scarified to a depth of at least 6 inches and compacted to at least 95 percent of standard Proctor maximum dry density (ASTM D 698) and within the range of 0 to 4 percentage points above the material's optimum moisture content.

5.7.2 Pavement Subgrade

Application Rate. Where lime stabilization is utilized, the exposed surface of the final pavement subgrade soil should be scarified to a depth of 6 inches and mixed with a minimum 7 percent hydrated lime (by dry soil weight) in conformance with TxDOT Standard Specifications Item 260. Assuming an in-place unit weight of 100 pcf for the pavement subgrade soils, this percentage of lime equates to about 32 lbs of lime per sq yard of treated subgrade. The actual amount of lime required should be confirmed by additional laboratory tests (ASTM C 977 Appendix XI) prior to construction. In all areas where hydrated lime is used to stabilize subgrade soil, routine Atterberg-limit tests should be performed to verify the resulting plasticity index of the soil-lime mixture is at/or below 15.

<u>Compaction.</u> The soil-lime mixture should be compacted to at least 95 percent of standard Proctor maximum dry density (ASTM D 698) and within the range of 0 to 4 percentage points above the mixture's optimum moisture content.

<u>Considerations.</u> Lime stabilization procedures should extend at least 1 ft beyond the edge of the pavement to reduce effects of seasonal shrinking and swelling upon the extreme edges of pavement. Lime stabilization of the pavement subgrade soil will not prevent normal seasonal movement of the underlying untreated materials. Pavement and other flat work will have the same potential for movement as slabs constructed directly on the existing undisturbed soils. As a minimum, good surface drainage and good perimeter drainage with a minimum slope of 2 percent away from the pavement is recommended. The use of sand as a leveling course below pavement and the use of an aggregate base course supported on expansive clays should be avoided. Normal maintenance of pavement should be expected over the life of the structures.

<u>Cautionary Note Regarding Stabilized Subgrades</u>. Stabilized subgrades are not suitable for supporting heavy construction traffic. Stabilized subgrades that have been subjected to heavy construction traffic should be re-inspected and re-stabilized as necessary prior to the construction of overlying pavement.

Note that this site is located in the Eagle Ford formation which can contain deposits of soluble sulfates. These compounds can react with lime and cause heaving of the pavement subgrade. Therefore, soluble sulfate testing of the pavement subgrade soils should be performed prior to mixing lime.

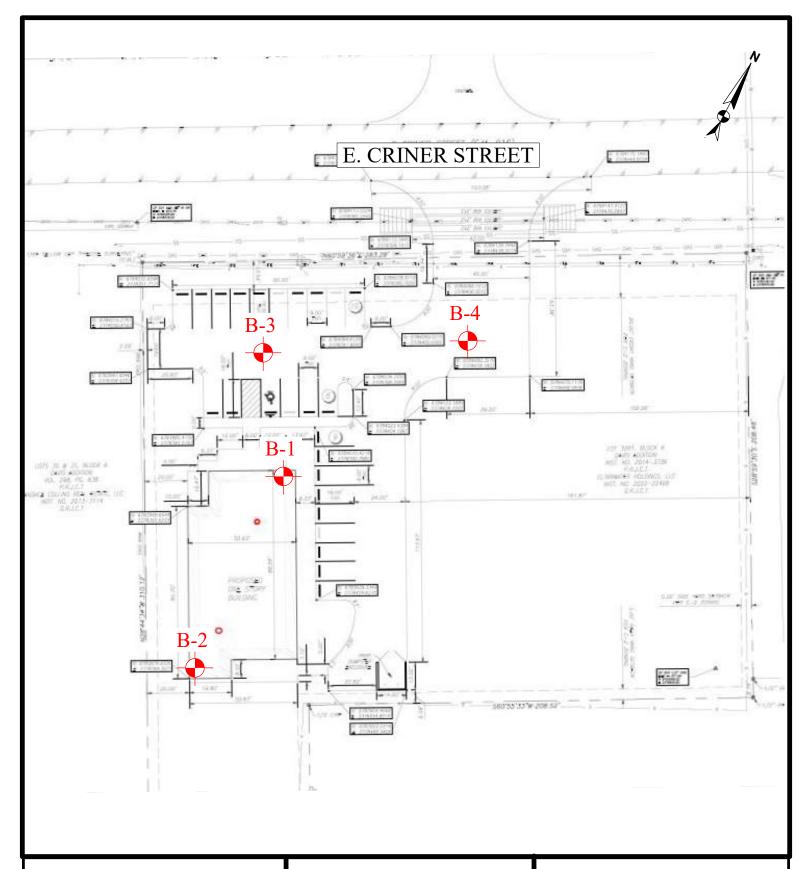
6.0 LIMITATIONS/GENERAL COMMENTS

Professional services provided in this geotechnical exploration were performed, findings obtained, and recommendations prepared in accordance with generally accepted geotechnical engineering principles and practices. The scope of services provided herein does not include an environmental assessment of the site or investigation for the presence or absence of hazardous materials in the soil, surface water or groundwater. UES, upon written request, can be retained to provide these services.

UES is not responsible for conclusions, opinions or recommendations made by others based on this data. Information contained in this report is intended for the exclusive use of the Client (and their designated design representatives), and is related solely to design of the specific structures No party other than the Client (and their designated design outlined in Section 2.0. representatives) shall use or rely upon this report in any manner whatsoever unless such party shall have obtained UES's written acceptance of such intended use. Any such third party using this report after obtaining UES's written acceptance shall be bound by the limitations and limitations of liability contained herein, including UES's liability being limited to the fee paid to it for this report. Recommendations presented in this report should not be used for design of any other structures except those specifically described in this report. In all areas of this report in which UES may provide additional services if requested to do so in writing, it is presumed that such requests have not been made if not evidenced by a written document accepted by UES. Further, subsurface conditions can change with passage of time. Recommendations contained herein are not considered applicable for an extended period of time after the completion date of this report. It is recommended our office be contacted for a review of the contents of this report for construction commencing more than one (1) year after completion of this report. Noncompliance with any of these requirements by the Client or anyone else shall release UES from any liability resulting from the use of, or reliance upon, this report.

Recommendations provided in this report are based on our understanding of information provided by the Client about characteristics of the project. If the Client notes any deviation from the facts about project characteristics, our office should be contacted immediately since this may materially alter the recommendations. Further, UES is not responsible for damages resulting from workmanship of designers or contractors. It is recommended the Owner retain qualified personnel, such as a Geotechnical Engineering firm, to verify construction is performed in accordance with plans and specifications.





GEOTECHNICAL EXPLORATION REPORT GRANDVIEW TEXAS VETERINARIAN CLINIC 802 EAST CRINER STREET GRANDVIEW, TEXAS UES PROJECT NO. W242089



FIGURE 1
BORING LOCATION PLAN

APPROXIMATE BORING LOCATION



BORING NO.: 1

PROJECT NO.: W242089

Client:	Location:			
Project:	ian Clinic	Surface Ele		
Start Date:	7/29/2024	End Date:	7/29/2024	West:
Drilling Method:	C	North:		

Location: Grandview, Texas

Surface Elevation: West: North:

D	Prilling	g Method:_	CONTINUOUS FLI	GHT AC	JGEF	Κ				Noi Hai	_	Drop	(lbs /	in):	170	/ 24	_ _
Depth, feet	Graphic Log		GROUND WATER OBSERVATIONS On Rods (ft): 15 After Drilling (ft): 15 After Hours (ft): MATERIAL DESCRIPTION	-	Sample Type	Recovery % RQD	TX Cone or Std. Pen. (blows/ft, in)	Pocket Penetrometer (tsf)	Unconfined Comp. Strength (tsf)	UU Shear Strength (tsf)	% Passing No. 200 Sieve	Unit Dry Weight (pcf)	Water Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Swell, %
	\prod	Dark Bi	rown CLAY with calcareous nodules					3.75					21				
				4.0				4.5					18	70	24	46	
_ 5 _	\prod		CLAY with calcareous nodules	6.0				4.5					20				
 	$ lap{II}$	Light B	rown CLAY with calcareous nodules					2.75					23				
 10	Щ			10.0				2.25					24	62	21	41	0.0
 		⊺an an∉	d Gray CLAY					3.0					27				
15	₩	▼ Tan an	d Gray SHALY CLAY	15.0													
 20 								3.0	1.5			98	19				
 			HALY CLAY with shale seams and	23.0													
 25 		layers TEST E	BORING TERMINATED AT 25 FT	25.0				4.5+					29				
_																	



BORING NO.: 2

Sheet 1 of 1

PROJECT NO.:_W242089

Client:		Location:	Grandview	, Texas			
Project: Grandview Texas Veterinarian C			ian Clinic	ation:	on:		
Start Date:	7/29/2024	End Date:	7/29/2024	West:			
Drilling Method:	C	CONTINUOUS FLIGHT AUGER					
				Hammer Drop	p (lbs / in):	170 / 24	

									паг	nmer	Drop	(IDS /	III):	-170	, 24	
Depth, feet	Graphic Log	GROUND WATER OBSERVATIONS On Rods (ft): NONE After Drilling (ft): DRY After Hours (ft): MATERIAL DESCRIPTION		Sample Type	Recovery % RQD	TX Cone or Std. Pen. (blows/ft, in)	Pocket Penetrometer (tsf)	Unconfined Comp. Strength (tsf)	UU Shear Strength (tsf)	% Passing No. 200 Sieve	Unit Dry Weight (pcf)	Water Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Swell, %
	\prod	Dark Brown CLAY	2.0				3.5					21				
	\prod	Brown CLAY with calcareous nodules	4.0				2.25					25	61	20	41	
_ 5 _	\prod	Light Brown CLAY with calcareous nodules	-				4.25					19				
			8.0				2.0					21				
10	\prod	Brown CLAY with calcareous nodules	10.0				2.5					20				
 		Tan CLAY	15.0				4.5+	2.2			94	26	79	26	53	
		Tan and Gray CLAY with shale					4.5+	2.0			91	26				
 	Ш	Gray SHALY CLAY	23.0			100/	4.5+					17				
25 		Gray SHALE TEST BORING TERMINATED AT 25 FT	25.0			100/ 2.50"										



BORING NO.: 3

Sheet 1 of 1

PROJECT NO.: W242089

Client:				Magee Architects		0"					Location: Grandview, Texas							
Project:		t:	7/29/2024	Grandview Texas Vete End Date:			nic 7/29/2				Surface Elevation:							
	rilling	g Method:	.,,_		HT AU						Nor	th:						_
		-									Har	Hammer Drop (lbs / in): 170 / 24						
Depth, feet	Graphic Log		GROUND WATER ▼ On Rods (ft): ▼ After Drilling (ft): ▼ After Hours MATERIAL DES	(ft):		Sample Type	Recovery % RQD	TX Cone or Std. Pen. (blows/ft, in)	Pocket Penetrometer (tsf)	Unconfined Comp. Strength (tsf)	UU Shear Strength (tsf)	% Passing No. 200 Sieve	Unit Dry Weight (pcf)	Water Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Swell, %
	Ш	Dark B	rown CLAY with calca						3.0					23				
 	₩	Brown	CLAY with calcareous	s nodules	2.0				4.5+					20	70	24	46	
5	Ш				5.0				3.0					22				
1015		TEST	BORING TERMINATE	ED AT 5 FT														



BORING NO.: 4

Sheet 1 of

PROJECT NO.: W242089

Grandview, Texas Client: Magee Architects Location: Grandview Texas Veterinarian Clinic Project: Surface Elevation: 7/29/2024 7/29/2024 End Date: Start Date: West: CONTINUOUS FLIGHT AUGER Drilling Method: North: 170 / 24 Hammer Drop (lbs / in): Pocket Penetrometer (tsf) Unconfined Comp. Strength (tsf) Unit Dry Weight (pcf) **GROUND WATER OBSERVATIONS** TX Cone or Std. Pen. (blows/ft, in) UU Shear Strength (tsf) Recovery % RQD Plasticity Index Sample Type Graphic Log Water Content, Liquid Limit Plastic Limit Depth, feet Swell, % On Rods (ft): DRY ▼After Drilling (ft): //After____ Hours (ft):_ MATERIAL DESCRIPTION Dark Brown CLAY with calcareous nodules 2.5 25 63 42 21 2.0 Brown CLAY with calcareous nodules 2.0 22 4.0 Light Brown CLAY with calcareous nodules 1.5 22 5.0 TEST BORING TERMINATED AT 5 FT 10 15 20



(SP), Poorly Graded SAND

KEY TO SOIL SYMBOLS AND CLASSIFICATIONS

RELATIVE PROPORTIONS (%)

PARTICLE SIZE IDENTIFICATION (DIAMETER)

SOIL & ROCK SYMBOLS RELATIVE DENSITY OF COHESIONLESS SOILS (blows/ft)

1			
(CH), High Plasticity CLAY	VERY LOOSE	0 TO 4	
	LOOSE	5 TO 10	
(CL), Low Plasticity CLAY	MEDIUM	11 TO 30	
	DENSE	31 TO 50	
(SC), CLAYEY SAND	VERY DENSE	OVER 50	

(SW), Well Graded SAND SHEAR STRENGTH OF COHESIVE SOILS (tsf)

(SM), SILTY SAND	VERY SOFT	LESS THAN 0.25
(OW), OILT TOTALE	SOFT	0.25 TO 0.50
(ML), SILT	FIRM	0.50 TO 1.00
(WE), SIET	STIFF	1.00 TO 2.00
(MH), Elastic SILT	VERY STIFF	2.00 TO 4.00
(WII 1), LIASTIC OIL 1	HARD	OVER 4.00

SHALE / MARL RELATIVE DEGREE OF PLASTICITY (PI)

	LOW	4 TO	15
SANDSTONE	MEDIUM	16 TO	25
(05) 5 1 0 1 105 115	HIGH	26 TO	35
(GP), Poorly Graded GRAVEL	VERY HIGH	OVER	35

GINI), SILTY GRAVEL		
	TRACE	1 TO 10
(OL), ORGANIC SILT	LITTLE	11 TO 20
	SOME	21 TO 35
(OH) ORGANIC CLAY	AND	36 TO 50

SAMPLING SYMBOLS

(GC), CLAYEY GRAVEL

LIMESTONE

		·	•
	SHELBY TUBE (3" OD except where noted otherwise)	BOULDERS COBBLES	8.0" OR LARGER 3.0" TO 8.0"
\times	SPLIT SPOON (2" OD except where noted otherwise)	COARSE GRAVEL	0.75" TO 3.0"
	noted otherwise)	FINE GRAVEL	5.0 mm TO 3.0"
	AUGER SAMPLE	COURSE SAND	2.0 mm TO 5.0 mm
		MEDIUM SAND	0.4 mm TO 5.0 mm
	TEXAS CONE PENETRATION	FINE SAND	0.07 mm TO 0.4 mm
$\overline{}$		SILT	0.002 mm TO 0.07 mm
	ROCK CORE (2" ID except where noted otherwise)	CLAY	LESS THAN 0.002 mm

SECTION 07 4113 METAL ROOF, WALL AND SOFFIT PANELS

PART 1 – GENERAL

1.01 SYSTEM DESCRIPTION

- A. Design Requirements; design roof system to withstand:
 - 1. Live and dead loads in accordance with Building Code.
 - 2. Minimum wind pressures in accordance with ASCE 7.
- B. Performance Requirements; Water leakage: None, tested to ASTM E 331 with test pressure of 6.24 PSF.

1.02 SUBMITTALS

- A. Submittals: Submit in accordance with Submittal Procedures.
 - 1. Shop Drawings: Show configuration of panels, trim members, and closures.
 - 2. Product Data: Show system components including panels, trim, and accessories.
 - 3. Samples: 3 x 3 inch finish samples showing available colors.
 - 4. Warranty: Sample warranty form.

1.03 QUALITY ASSURANCE

A. Installer Qualifications: Minimum 5 years documented experience in work of this section.

1.04 DELIVERY, STORAGE AND HANDLING

A. Protect panels from contact with materials that could cause staining or discoloration of finish.

1.05 PROJECT CONDITIONS

- A. Do not install underlayment at ambient or surface temperatures less than 40 degrees F or on wet or frozen substrate.
- B. Do not install panels on wet or frozen substrate.

1.06 WARRANTIES

A. Furnish manufacturer's 20-year warranty providing coverage against chipping, cracking, fading, or delamination of panel finish.

PART 2 - PRODUCTS

2.01 MANUFACTURERS

- A. Manufacturer: Sheffield Metals Snap-Lock as Basis-of-Design (www.sheffieldmetals.com)
- B. Acceptable Manufacturers:
 - 1. AEP-Span. (www.aep-span.com)
 - 2. Berridge Manufacturing Co. (www.berridge.com)
 - 3. Centria Architectural Systems. (www.centria.com)
 - 4. Fabral. (www.fabral.com)
 - 5. MBCI. (www.mbci.com)
 - 6. Petersen Aluminum Corp. (www.pac-clad.com)

2.02 MATERIALS

- A. Galvanized Steel Sheet: ASTM A653, Structural Quality, G90 coating class.
- B. Underlayment: Tamko TW Metal and Tile underlayment, ASTM D1970, fiberglass reinforced, self-adhering rubberized asphalt sheet membrane.
- C. Metal Mesh Panels: Expanded Metal, Stainless Steel Type 316, 1/2 #16 Flattened, 60% Open Area, Sheet, 48.0000" Width x 96.0000" Length, Long Way of Opening Parallel to: Length, Metal Wall Panels applied as the cladding over wall framing specified in 05 4000 Cold-Formed Metal Framing.
- D. Accent Metal Panels: Grade 80 full hard steel, corrugated galvanized metal panels.

2.03 ACCESSORIES

- A. Fasteners:
 - 1. Underlayment: Plastic-capped Hot-dip galvanized steel nails (as needed), length to penetrate minimum 3/4 inch into sheathing.
 - 2. Panels and Trim: 300 Series stainless steel, type best suited to application; head color to match panels where exposed, with neoprene gasketed washers.
- B. Panel Clips: Hot-dip galvanized steel, designed to fit between two adjacent panels and secure both panels.
- C. Panel End Closures: Sponge neoprene, cut to fit panel configuration, minimum 1 inch depth.
- D. Joint Sealers: Specified in Section 07 9200.

2.04 FABRICATION

- A. Fabricate panels from minimum 24 gage galvanized steel sheet.
- B. <u>Standing-seam Panel Profile</u>: 2 inch high standing seams spaced 12 to 16 inches on center with interlocking edges (Optional Mechanically Seamed).
- C. <u>Wall & Soffit Panel Profile</u>: 12" wide by 1-1/2" depth with Exposed Fasteners with Screw Caps on <u>Wall Panels</u> & Concealed Fasteners and interlocking sidelap on <u>Soffit Panels</u>. Profile shall have two vee grooves spaced at 4" o.c., vented panels, factory formed, continuous lengths.
 - 1. Panel Attachment: Concealed clips,
 - 2. Panel Substrate: 3/4" Plywood, C-D/Exposure 1-APA, Rated Sheathing 16/0 span rating.
 - 3. Exterior Panel Finish: Smooth, Flat Finish.
 - 4. Interior Panel Finish: Smooth, Flat Finish.
 - 5. Exterior Panel Gauge: 24.
- D. Trim: Profiles as indicated or as required, fabricated from same material as panels.
- E. Roll form panels and trim to required profiles in longest practical lengths.

2.05 FINISHES

A. Panels and Trim: Fluoropolymer coating, AAMA 2605, containing minimum 70 percent PVDF resins applied to sheets in coil form, color to be galvalume.

PART 3 - EXECUTION

3.01 INSTALLATION OF UNDERLAYMENT

- A. Starting at low edge, apply one ply of underlayment horizontally over substrate.
- B. Weather lap each strip 6 inches minimum over previous strip.

- C. Lap ends 6 inches minimum.
- D. Fasten top of each strip under overlapping strip to hold strip in position until roofing panels are installed.
- E. Provide 18 inch weave pattern at valleys.
- F. Lap underlayment minimum 12 inches over hips and ridges from both sides. Apply 36 inch wide strip centered lengthwise over ridge. Nail at 12 inches on center on each side.
- G. Extend minimum 4 inches up abutting vertical surfaces.

3.02 INSTALLATION OF METAL PANELS

- A. Install in strict accordance with manufacturer's written instructions and recommendations.
- B. Install aligned, level, and plumb.
- C. Fasten panels using concealed panel clips.
- D. Install panels in continuous lengths from eave to ridge without end joints.
- E. Install trim to maintain visual continuity of system.
- F. Install joint sealers and gaskets to prevent water penetration.
- G. Flash penetrations through roofing with metal trim to match panels:
 - 1. Lap flashings over roof panels 12 inches minimum on all sides and seal with double bead of joint sealer
 - 2. Install metal draw band and joint sealer at top of pipe penetrations.
 - 3. Install water diverter at uphill side of square and rectangular penetrations.
- H. Installation Tolerances:
 - 1. Variation from location: Plus or minus 1/4 inch.
 - 2. Variation from plane: 1/4 inch in 10 feet.

3.03 CLEANING AND PROTECTION

- A. Remove temporary protective coverings and strippable films, if any, as metal panels are installed, unless otherwise indicated in manufacturer's written installation instructions. On completion of metal panel installation, clean finished surfaces as recommended by metal panel manufacturer. Maintain in a clean condition during construction.
- B. After metal panel installation, clear weep holes and drainage channels of obstructions, dirt, and sealant.
- C. Replace metal panels that have been damaged or have deteriorated beyond successful repair by finish touchup or similar minor repair procedures.

3.04 ADJUSTING

A. Touch up field cuts and abrasions on finished surfaces to match factory finish.

END OF SECTION

SECTION 09 6723 RESINOUS FLOORING

PART 1 – GENERAL

1.01 RELATED DOCUMENTS

A. Drawings and general provisions of the Contract, including General and Supplementary Conditions and Division 01 Specification Sections, apply to this Section.

1.02 SUMMARY

- A. Section Includes:
 - 1. Dur-A-Flex, Inc Dur-A-Gard, Epoxy-Based seamless flooring system
- B. Related Sections:
 - 1. Section 03 3000 Cast-in-Place Concrete.
 - 2. Section 07 9200 Joint Sealants for sealants installed at joints in resinous flooring systems.

1.03 SYSTEM DESCRIPTION

A. The work shall consist of preparation of the substrate, the furnishing and application of a pigmented epoxy-based floor coating system. The system shall have the color and texture as specified by the Owner with a nominal thickness of 40mils. It shall be applied to the prepared area(s) as defined in the plans strictly in accordance with the Manufacturer's recommendations.

1.04 SUBMITTALS

- A. Product Data: Latest edition of Manufacturer's literature including performance data and installation procedures.
- B. Manufacturer's Safety Data Sheet (SDS) for each product being used.
- C. Samples: A 3 x 3-inch square sample of the proposed system. Color, texture, and thickness shall be representative of overall appearance of finished system subject to normal tolerances.

1.05 QUALITY ASSURANCE

- A. The Manufacturer shall have a minimum of 10 years' experience in the production, sales, and technical support of epoxy and urethane industrial flooring and related materials.
- B. The Applicator shall have been approved by the flooring system manufacturer in all phases of surface preparation and application of the product specified.
- C. No requests for substitutions shall be considered that would change the generic type of the specified System.
- D. System shall be in compliance with requirements of United States Department of Agriculture (USDA),
 Food, Drug Administration (FDA), and local Health Department.
- E. A pre-installation conference shall be held between Applicator, General Contractor and the Owner to review and clarification of this specification, application procedure, quality control, inspection and acceptance criteria and production schedule.

1.06 PRODUCT DELIVERY, STORAGE, AND HANDLING

- A. Packing and Shipping:
 - 1. All components of the system shall be delivered to the site in the Manufacturer's packaging, clearly identified with the product type and batch number.

B. Storage and Protection

- 1. The Applicator shall be provided with storage area for all components. The area shall be between 60 F and 90 F, dry, out of direct sunlight and in accordance with the Manufacturer's recommendations and relevant health and safety regulations.
- Copies of Safety Data Sheets (SDS) for all components shall be kept on site for review by the Engineer or other personnel.

C. Waste Disposal

1. The Applicator shall be provided with adequate disposal facilities for non-hazardous waste generated during installation of the system.

1.07 PROJECT CONDITIONS

A. Site Requirements:

- Application may proceed while air, material and substrate temperatures are between 60 F and 90 F
 providing the substrate temperature is above the dew point. Outside of this range, the Manufacturer
 shall be consulted.
- 2. The relative humidity in the specific location of the application shall be less than 85% and the surface temperature shall be at least 5 F above the dew point.
- 3. The Applicator shall be supplied with adequate lighting equal to the final lighting level during the preparation and installation of the system.
- B. Conditions of new concrete to be coated with epoxy material.
 - Concrete shall be moisture cured for a minimum of 7 days and have fully cured a minimum of twenty eight days in accordance with ACI-308 prior to the application of the coating system pending moisture tests.
 - 2. Concrete shall have a flat rubbed finish, float, or light steel trowel finish (a hard steel trowel finish is neither necessary nor desirable).
 - 3. Sealers and curing agents should not be used.
 - 4. Concrete surfaces on grade shall have been constructed with a vapor barrier to protect against the effects of vapor transmission and possible delamination of the system.

C. Safety Requirements

- 1. All open flames and spark-producing equipment shall be removed from the work area prior to commencement of application.
- 2. "No Smoking" signs shall be posted at the entrances to the work area.
- 3. The Owner shall be responsible for the removal of foodstuffs from the work area.
- 4. Non-related personnel in the work area shall be kept to a minimum.

1.08 WARRANTY

- A. Dur-A-Flex, Inc. warrants that material shipped to buyers at the time of shipment substantially free from material defects and will perform substantially to Dur-A-Flex, Inc. published literature if used in accordance with the latest prescribed procedures and prior to the expiration date.
- B. Dur-A-Flex, Inc. liability with respect to this warranty is strictly limited to the value of the material purchase.

PART 2 - PRODUCTS

2.01 FLOORING

- A. Dur-A-Flex, Inc, Dur-A-Gard, Epoxy-Based seamless flooring system
 - 1. System Materials:
 - a. Primer: Dur-A-Flex, Inc, Elast-O-Coat resin and hardener.
 - b. Base Coat: Dur-A-Flex, Inc, Dur-A-Gard resin and hardener.
 - c. Topcoat: Dur-A-Flex, Inc. Armor Top pigmented resin and hardener and pigment.
 - 2. Patch Materials:
 - a. Shallow Fill and Patching: Use Dur-A-Flex, Inc. Dur-A-Glaze #4 Cove Rez.
 - b. Deep Fill and Sloping Material (over ¼ inch): Use Dur-A-Flex, Inc. Dur-A-Crete.

2.02 MANUFACTURER

- A. Dur-A-Flex, Inc., 95 Goodwin Street, East Hartford, CT 06108, Phone: (860) 528-9838, contact_us@dur-a-flex.com
- B. Manufacturer of Approved System shall be single source and made in the USA.

2.03 PRODUCT REQUIREMENTS

A.	Primer		Elast-O-Coat					
	1. Percent Solids		100 %					
	2. VOC		4.34 g/L					
	3. Elongation, ASTMD 412		150 %					
	4. Tensile Strength, ASTM D 412		2,400 psi					
B.	Base Coat	Ε	Our-A-Gard					
	1. Percent Solids		100 %					
	2. VOC		4 g/L					
	3. Compressive Strength, ASTM D 695	16,000 psi						
	4. Tensile Strength, ASTM D 638		3,000 psi					
	5. Flexural Strength, ASTM D 790		4,000 psi					
	6. Abrasion Resistance, ASTM D 4060							
	CS 17 Wheel, 1,000 gm load, 1,000 cycles		35 mg loss					
	7. Flame Spread/NFPA-101, ASTM E 84		Class A					
	8. Flammability, ASTM D 635		Self Extinguishin	ng				
	9. Impact Resistance MIL D-3134		0.025-inch Max					
	10. Water Absorption. ASTOM D 570		0.04 %					
	11. Pot Life @ 70 F		20-25 minutes					
C.	Topcoat		Armor Top					
	1. Percent Solids		95.2 %					
	2. VOC		0 g/L					
	3. Tensile Strength, ASTM D 2370		7,000 psi					
	4. Adhesion, ASTM 4541		Substrate Failur	e				
	5. Hardness, ASTM D 3363		>4H					
	6.600 Gloss ASTM D 523		Satin 50+/-10	Gloss 70+/-10				
	7. Abrasion Resistance, ASTM D4060	Gloss	Satin					
	09 6723- 3							

CS 17 wheel (1,000 g load) 1,000 cycles
4 8 mg loss with grit
10 12 mg loss without grit
8. Pot Life, 70 F, 50% RH
45 mins
9. Full Chemical Resistance
7 days

PART 3 - EXECUTION

3.01 EXAMINATION

- A. Examine substrates, areas and conditions, with Applicator present, for compliance with requirements for maximum moisture content, installation tolerances and other conditions affecting flooring performance.
 - Verify that substrates and conditions are satisfactory for flooring installation and comply with requirements specified.

3.02 PREPARATION

A. General:

- 1. New and existing concrete surfaces shall be free of oil, grease, curing compounds, loose particles, moss, algae growth, laitance, friable matter, dirt, and bituminous products.
- 2. Moisture Testing: Perform tests recommended by manufacturer and as follows.
 - a. Perform anhydrous calcium chloride test ASTM F 1869-98. Application will proceed only when the vapor/moisture emission rates from the slab is less than and not higher than 3 lbs/1,000 sf/24 hrs.
 - b. Perform relative humidity test using in situ probes, ASTM F 2170. Proceed with installation only after substrates have a maximum 75% relative humidity level measurement.
 - c. If the vapor emission exceeds 75 % relative humidity or 3 lbs/1,000 sf/24 hrs. then Dur-A-Flex, Inc Dur-A-Glaze MVP Primer moisture mitigation system must be installed prior to resinous flooring installation. Slab-on grade substrates without a vapor barrier may also require the moisture mitigation system.
- 3. There shall be no visible moisture present on the surface at the time of application of the system.

 Compressed oil-free air and/or a light passing of a propane torch may be used to dry the substrate.
- 4. Mechanical surface preparation
 - a. Shot blast all surfaces to receive flooring system with a mobile steel shot, dust recycling machine (Blastrac or equal). All surface and embedded accumulations of paint, toppings hardened concrete layers, laitance, power trowel finishes, and other similar surface characteristics shall be completely removed leaving a bare concrete surface having a minimum profile of CSP 2-3 as described by the International Concrete Repair Institute.
 - b. Floor areas inaccessible to the mobile blast machines shall be mechanically abraded to the same degree of cleanliness, soundness and profile using diamond grinders, needle guns, bush hammers, or other suitable equipment.
 - c. Where the perimeter of the substrate to be coated is not adjacent to a wall or curb, a minimum 1/8-inch key cut shall be made to properly seat the system, providing a smooth transition between areas. The detail cut shall also apply to drain perimeters and expansion joint edges.
 - d. Cracks and joints (non-moving) greater than 1/8-inch wide are to be chiseled or chipped-out and repaired per manufacturer's recommendations.
- 5. At spalled or worn areas, mechanically remove loose or delaminated concrete to a sound concrete and patch per manufactures recommendations.

3.03 APPLICATION

A. General:

- 1. The system shall be applied in four distinct steps as listed below:
 - a. Substrate preparation
 - b. Priming
 - c. Base coat application.
 - d. Topcoat application
- Immediately prior to the application of any component of the system, the surface shall be dry, and any remaining dust or loose particles shall be removed using a vacuum or clean, dry, oil-free compressed air.
- 3. The handling, mixing and addition of components shall be performed in a safe manner to achieve the desired results in accordance with the Manufacturer's recommendations.
- 4. The system shall follow the contour of the substrate unless pitching or other leveling work has been specified by the Architect.
- 5. A neat finish with well-defined boundaries and straight edges shall be provided by the Applicator.

B. Membrane

- 1. The Elast-O-Coat membrane shall consist of a liquid resin and hardener that is mixed at the ratio of 2 parts resin to 1 part hardener per the manufacturer's instructions.
- 2. The Elast-O-Coat membrane shall be applied by flat squeegee and back rolled at the rate of 80 sf/gal to yield a dry film thickness of 20 mils.

C. Base Coat

- 1. The base coat shall be comprised of two component Dur-A-Gard, a resin, and hardener as supplied by the Manufacturer.
- 2. The resin shall be added to the hardener and thoroughly mixed by suitably approved mechanical means.
- 3. The base coat shall be applied over horizontal surfaces using "v" notched squeegee and back rolled at the rate of 100 sf/gal to yield a dry film thickness of 16 mils.

D. Topcoat

- 1. The topcoat shall be comprised of three components, a resin, hardener, and pigment as supplied by the Manufacturer.
- 2. The resin and pigment shall be added to the hardener and thoroughly mixed by suitably approved mechanical means.
- 3. The topcoat shall be applied over horizontal surfaces at the rate of 500 sf/gal to yield a dry film thickness of 3-4 mils.
- 4. The finish floor will have a nominal thickness of 40 mils.

3.04 FIELD QUALITY CONTROL

- A. Tests, Inspection
 - 1. The following tests shall be conducted by the Applicator:
 - a. Temperature
 - 1) Air, substrate temperatures and, if applicable, dew point.
 - b. Coverage Rates

1) Rates for all layers shall be monitored by checking quantity of material used against the area covered.

3.05 CLEANING AND PROTECTION

- A. Cure flooring material in compliance with manufacturer's directions, taking care to prevent their contamination during stages of application and prior to completion of the curing process.
- B. Remove masking. Perform detail cleaning at floor termination, to leave cleanable surface for subsequent work of other sections.

END OF SECTION

SECTION 31 3213 CHEMICAL SOIL STABILIZATION

PART 1 – GENERAL

1.01 SUBMITTALS

A. Submittals: Submit in accordance with Section 01 3300 - Submittal Procedures.

1.02 QUALITY ASSURANCE

- A. The details of the injection/application rate, injection pressure, and chemical concentration to provide uniform distribution of the chemical mixture will be determined solely by the applicator.
- B. Installer Qualifications: A firm with not less than 10 years successful experience in chemical soil injection and quality control and shall have been in business under the same name and operating as a soil stabilization company for not less than 10 years.

PART 2 - PRODUCTS

2.01 CHEMICAL INJECTION STABILIZATION MATERIALS

- A. Soil: Upper 15'-0" of material in place after the subgrade below the pavement has been established and shaped.
- B. Chemical: EcSS 3000 as manufactured by Environmental ® Soil Stabilization, L.L.C. (phone 817.426.8000 web site: www.esslsoils.com), or approved equal. Equivalent chemical shall be shown to be able to reduce the swell characteristics of the in-place clays to meet the project specifications and be shown to not only reduce the negative charge of the clay particles but to also change the clay structure from an expanding crystalline lattice to a non-crystalline, amorphous structure.
 - Equivalent products and application processes, subject to all requirements of the drawings and specifications, as manufactured by ProChemical Soil Stabilization of Texas (phone 817.832.6223 web site: www.prochemtex.com)

2.02 EQUIPMENT

A. Equipment shall be suitable for the intended work. Injection equipment shall be self-propelled and constructed to provide straight pipe injection under pressure to the stated treatment depth. Injection equipment shall be equipped with flow meter and pressure meter and control valve for monitoring and controlling the amount of chemical injected. The pump units shall have centrifugal pumps installed and shall be capable of injecting at least 7,500 gallons/hour at 200 to 250 pounds per square inch constant pressure.

PART 3 - EXECUTION

3.01 PREPARATION

A. The area to be chemical injected shall be graded to subgrade required for pavement thickness indicated.

B. Swelling the active clays shall be anticipated during the chemical injection process. Additional grading of the site may be required prior to paving.

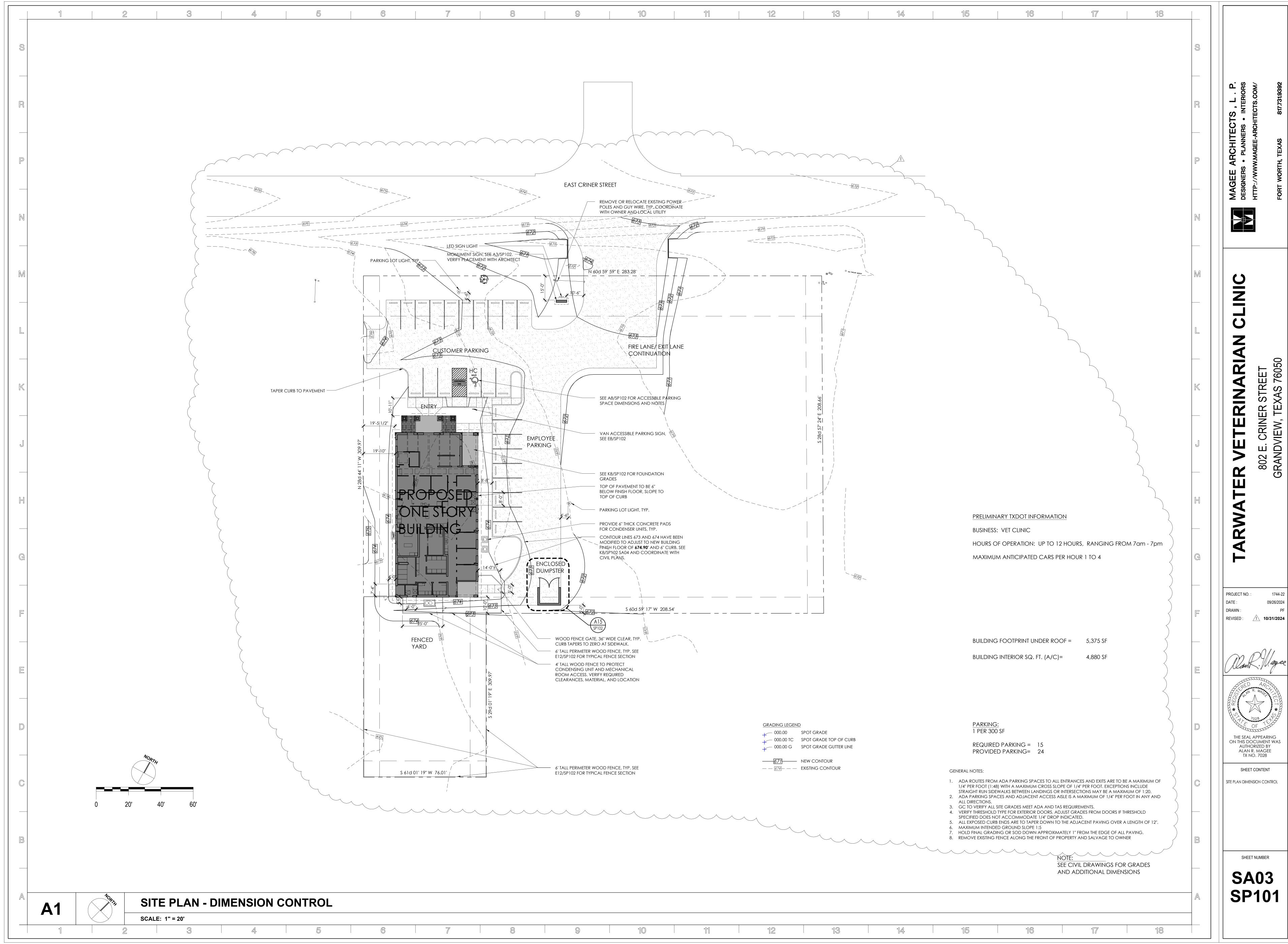
3.02 CHEMICAL INJECTION APPLICATION

- A. The subgrade shall be injected to a depth of 15 feet and at least 5 feet beyond the paving limits. Injection rods shall be forced downward (not jetted or washed) in approximately 12 inch vertical intervals, to a depth of 15 feet. Spacing for the injection holes shall not exceed 3 feet on center, each way. Injection shall be carried outside paving limits a minimum of 5 feet.
- B. A minimum waiting period of 72 hours is required before finishing operations, sampling, or testing is performed.

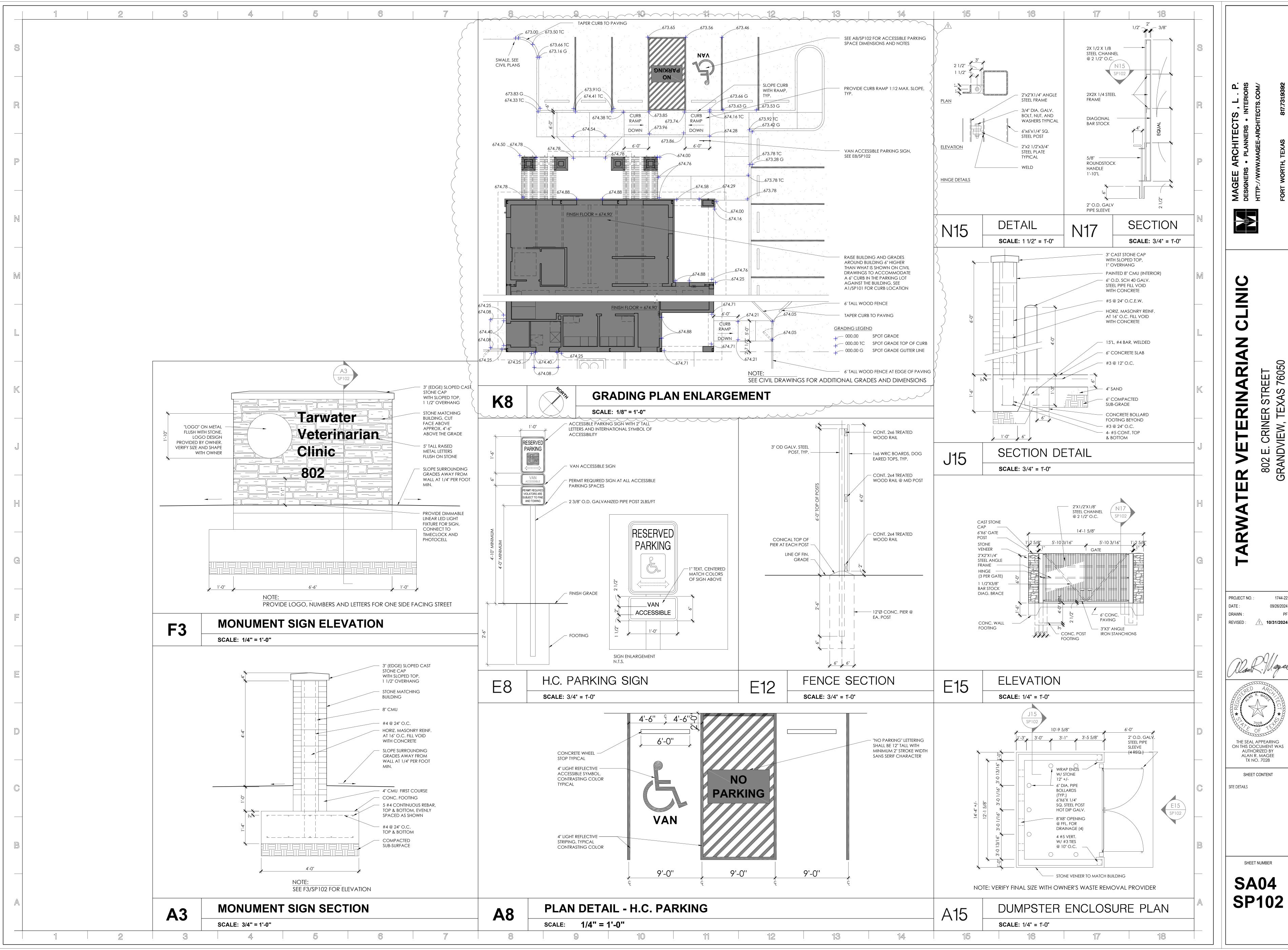
3.03 FIELD QUALITY CONTROL

- A. Post-treatment evaluation for chemical injection shall be based on one dimensional laboratory swell tests (ASTM D 4546, Method B) conducted by the Owner's geotechnical engineer. Soil samples used for testing shall be undisturbed samples retrieved by using thin walled seamless tube samplers to a depth equal to the specified injection depth.
- B. Sampling shall be one sample for each 5,000 to 10,000 square feet, or portion thereof, of treated area, or a minimum of 2 sample borings, whichever is greater. Sample borings shall be taken at an equal distance from injection points. Continuous tube samples shall be obtained from the entire treated depth. Samples shall be extruded from the sampling tube, wrapped in plastic, sealed in plastic bags to prevent moisture loss, and protected from disturbance. Aluminum foil shall not be used.
- C. A minimum of 4 one-dimensional swell tests shall be performed for each sample boring for injection depths up to 15 feet. Test depth ranges shall be: 0 to 3 feet, 3 to 5 feet, 5 to 7 feet, 7 to 10 feet, and 10 to 15 feet. One dimensional swell tests shall be documented in accordance with ASTM D 4546, Method B. Test results shall be reported for a swell of 48 hours duration under a single surcharge load simulating overburden pressure after construction of the pavement. The swell test shall be continued beyond 48 hours if the sample exhibits a 25 percent or greater change in sample height during the 36 to 48 hour test interval. Moisture and hand penetrometer determinations shall be performed on one foot intervals in all borings.
- D. The average swell from each boring sampled shall not exceed 1.0 percent; and no swell test from each boring shall have a swell of more than 2.0 percent.
- E. Where the swell criteria is not met in any one of the borings, determination of the project area and depth increment to be re-injected will be made by the geotechnical engineer. Re-treatment and acceptance testing will be performed in accordance with the geotechnical engineer's recommendations.

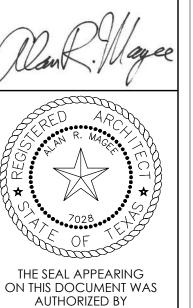
END OF SECTION



COPYRIGHT © 2024, MAGEE ARCHITECTS, L.P.



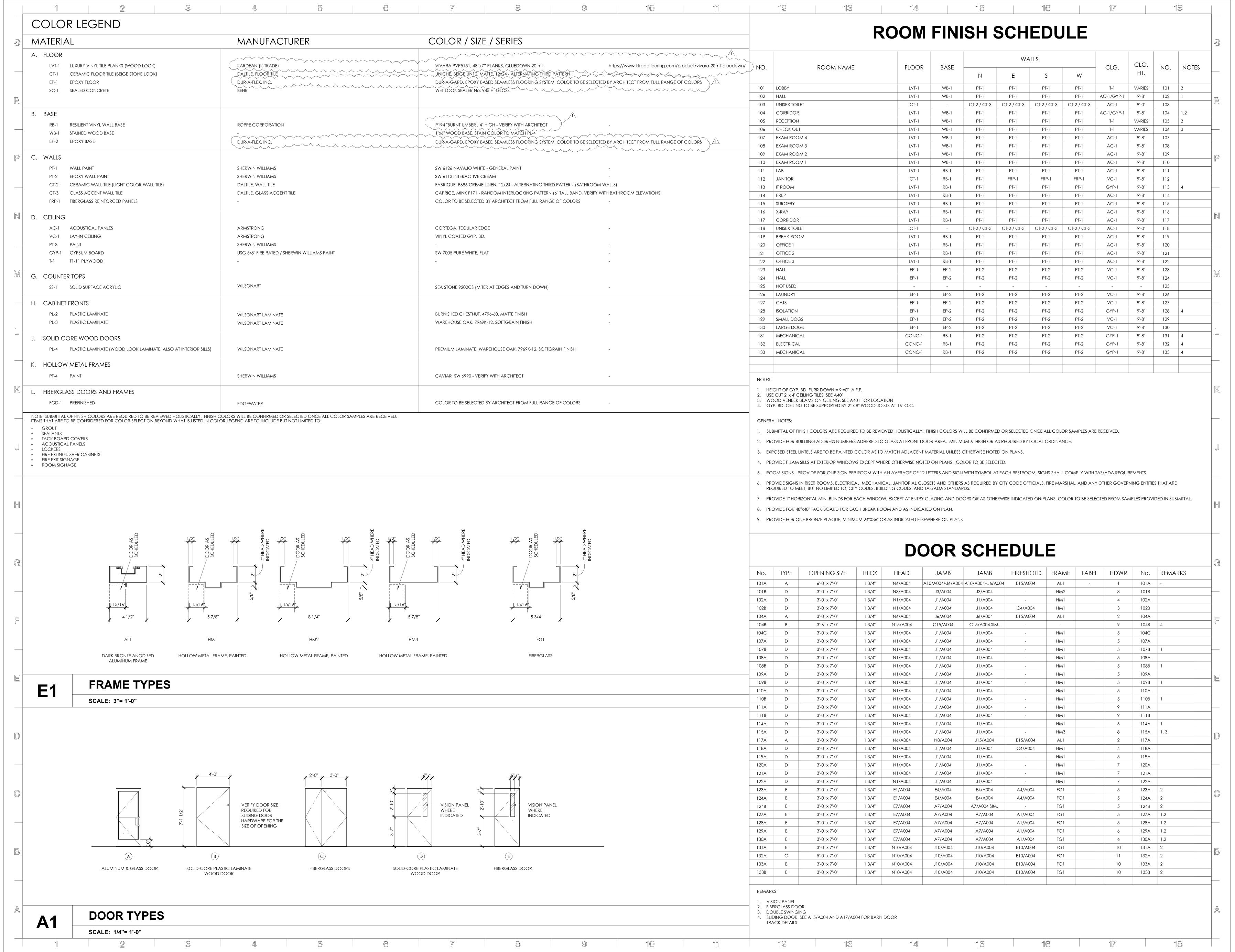
PROJECT NO.: 10/31/2024 REVISED:



ALAN R. MAGEE TX NO. 7028 SHEET CONTENT

SHEET NUMBER **SA04**

COPYRIGHT © 2024, MAGEE ARCHITECTS, L.P.



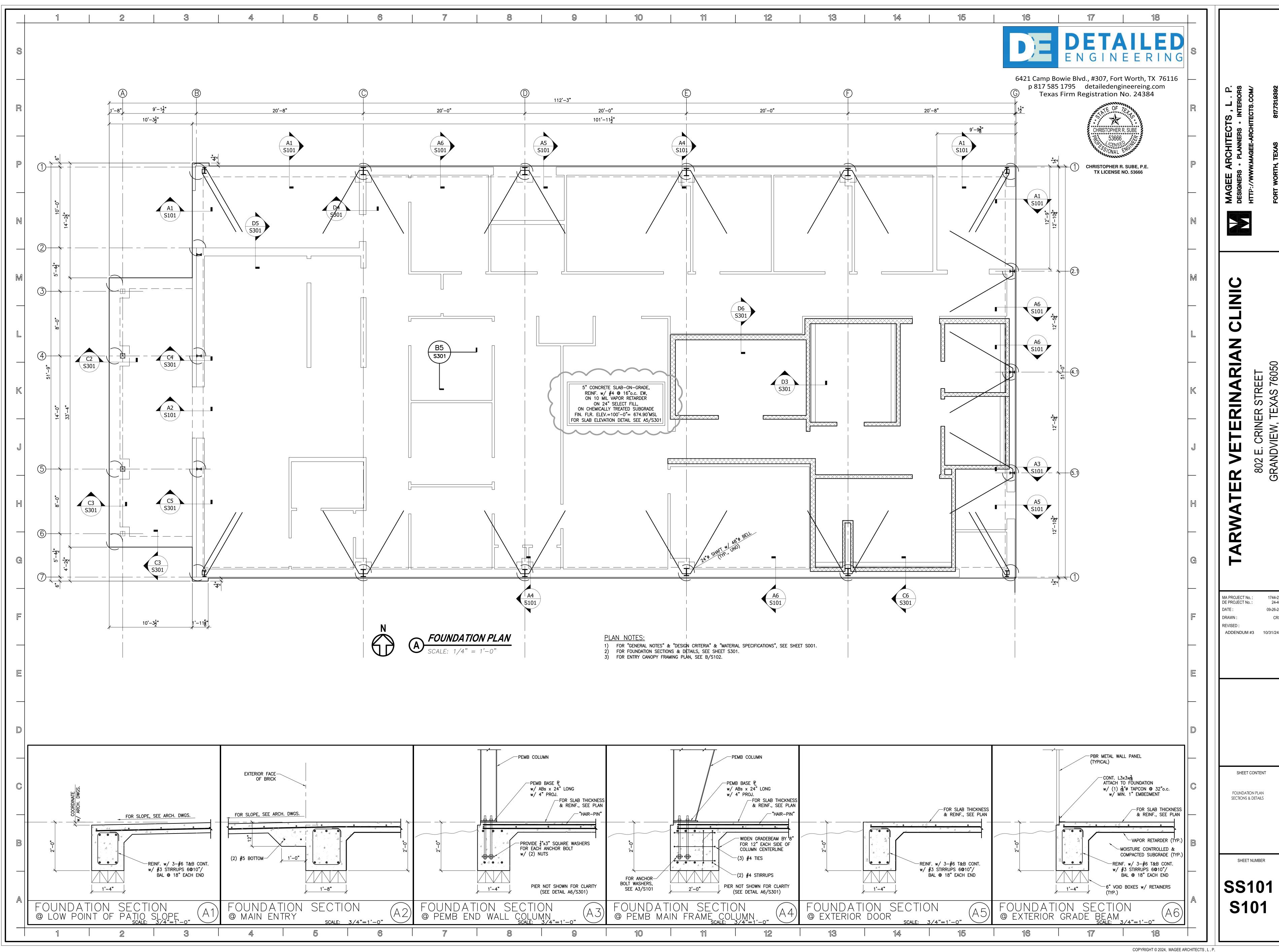
COPYRIGHT © 2024, MAGEE ARCHITECTS, L.P.

PROJECT NO.: REVISED:

1 10/31/2024

AUTHORIZED BY ALAN R. MAGEE TX NO. 7028

SHEET CONTENT ROOM FINISH SCHEDULE, COLOR LEGEND, DOOR SCHEDULE, TYPES WINDOW TYPES WINDOW DETAILS



SHEET CONTENT FOUNDATION PLAN

SHEET NUMBER

SS101 S101

1. EXTERNAL STATIC PRESSURE ("WG") INCLUDES DUCTWORK, BALANCING DAMPERS AND AIR DEVICES ONLY

2. CAPACITIES LISTED ARE NET FROM UNIT DISCHARGE. UNITS SHALL PERFORM TO LISTED CAPACITIES. UNIT PERFORMANCE MUST SATISFY BOTH SENSIBLE AND LATENT CAPACITY REQUIREMENTS.

3. PROVIDE FACTORY CONDENSER COIL HAIL GUARDS.

4. PROVIDE WITH MODULATING ELECTRIC HEAT (SCR).

5. PROVIDE WITH CRANKCASE HEATER.

6. PROVIDE WITH MODULATING VFD DRIVEN COMPRESSOR

7. AAON IS THE BASIS OF DESIGN. NO EXCEPTIONS.

8. PROVIDE WITH AAON CONTROLLER WITH PROGRAMMING TO SUPPORT BOTH TEMPERATURE AND HUMIDITY CONTROL.

9. PROVIDE UNIT WITH MODULATING ELECTRIC REHEAT (SCR).

														SPLIT	SYSTE	M SCI	HEDU	JLE													
		INDOOR UNIT								AIR COOLED CONDENSING UNIT								FCU (FCU COOLING PERFORMANCE DATA												
MARK	TONNAGE		UNIT	O/A	EXT.		F	OWER	CONNECT	ION			COM	PRESSORS	REF.	FANS			POWER			HEATING	CAPACITY			CAPA	ACITY	AMB.	ENTF	ERING	REMARKS
IVIARK	IONNAGE	ARRANGEMENT	CFM	CFM	S.P.	H.P.	V	Dh	CIRC	CUIT 1	WEIGHT/LBS	MANUFACTURER AND MODEL NO.	NO.	R.L.AMPS	TYPE	NO. F	:I A	(CONNECTION	NC	O.D.	I.D. DB	LVG DB	MDU	MANUFACTURER AND MODEL NO.	(ME	BH)	D.B.	D.B.	W.B.	REWARKS
							V.	Pn.	MCA	МОСР		7413 1110322 1101	NO.	EACH		NO. F	LA	V. F	Ph. MCA	MOCP	TEMP	TEMP	TEMP	IVIDII		TOTAL	SENS	F.	F.	F.	
AHU/CU-1	3	VERTICAL	980	200	0.4	1/2	208	31	5.0	15.0	144	TRANE/TEM6	1	17.0	R410A	1 0.	.74	208	1 24	35	22	60	85	26.2	TRANE/4TWR	33.1	27.6	105	81	68	1-10
AHU/CU-2	5	VERTICAL	1,740	350	0.7	3/4	208	3 1	9.0	15.0	174	TRANE/TEM6	1	32.1	R410A	1 1	1.3 🥤	208	1 41	60	22	60	85	46.3	TRANE/4TWR	58.9	47.0	105	81	68	1-10
AHU/CU-4	1.5	WALL MOUNTED	437	0			208	31	1.0		29	MITSUBISHI/MSZ	1	17.0	R410A	1 0	.65	208	1 18	20	22	75	95	9.4	MITSUBISHI/MUZ	16.4	10.9	105	78	62	2-9, 11-13
AHU/CU-5	1	WALL MOUNTED	400	0	-	-	208	1	1.0	-	22	MITSUBISHI/MSY	1	17.0	R410A	1 0.	.65	208	1 7	15	-	-	-	-	MITSUBISHI/MUY	9.0	9.0	105	78	62	2-9, 11-13
REMARKS:	······································																														

1. UNITS SHALL BE PROVIDED WITH TXV VALVES

2. SIZE, ROUTE, INSULATE AND PROVIDE APPURTENANCES FOR DX PIPING SYSTEMS, IN STRICT ACCORDANCE WITH MANUFACTURER'S PUBLISHED INSTRUCTIONS.

3. LISTED CAPACITIES ARE FOR THE FAN COIL UNIT AND CONDENSER UNIT COMBINATION. UNITS SHALL PERFORM TO LISTED CAPACITIES.

4. PROVIDE FACTORY CONDENSER COIL HAIL GUARDS.

5. SEER / EER. RATINGS ARE AT ARI CONDITIONS FOR CONDENSING UNIT ONLY.

6. PROVIDE FILTER DRYER AND SIGHT GLASS ON THE DX LINES.

7. FOR LONG DX RUNS, USE MANUFACTURER'S RECOMMENDED LONG LINE INSTALLATION GUIDELINES.

8. PROVIDE FACTORY PROGRAMMABLE THERMOSTAT 7-DAY, 2-EVENT.

9. COORDINATE OUTDOOR UNIT MOUNTING REQUIREMENTS.

10. ACCEPTABLE MANUFACTURERS ARE: CARRIER, LG, DAIKIN, TRANE, MITSUBISHI.

11. PROVIDE WITH AN MINI CONDENSATE PUMP. 12. ACCEPTABLE MANUFACTURERS ARE: MITSUBISHI, LG.

13. THE INDOOR UNIT IS POWERED BY THE OUTDOOR UNIT.

				FAN SCH	EDULE			
MARK	SERVES	CFM	EXT. SP	MOTOR DATA	DRIVE	MAX	WEIGHT/LBS	MANUFACTURER/

MARK	CEDVEC	CFM	EXT. SP	MOTOR DATA			DRIVE	MAX	WEIGHT/LBS	MANUFACTURER/	REMARKS
EF-	SERVES	CFIVI	IN WG	HP	VOLTS	PH	DRIVE	SONES	WEIGHT/LBS	MODEL SERIES	REWARKS
1-6	RESTROOMS & EXAM ROOMS	50	0.3	1/25	120	1	DIRECT	10.2	12	COOK/GC-128	1,2,3
7	PREP ROOM	830	0.3	1/3	120	1	DIRECT	4.0	58	COOK/GC-822	1,2,4
8	ANIMAL ZONES	780	0.5	1/5	120	1	DIRECT	9.5	49	COOK/100 SQN-D GALV	1,2,5

1. ACCEPTABLE MANUFACTURER'S ARE: LOREN COOK, GREENHECK, PENNBARRY.

2. PROVIDE VIBRATION ISOLATORS.

3. FAN RUNS INTERMITTENTLY, CONTROLED BY THE ATTACHED OCCUPANCY SENSOR.

4. FAN RUNS INTERMITTENTLY, CONTROLED BY A SWITCH WITH A PROGRAMMABLE TIMER. 5. FAN RUNS CONTINUOUSLY.

	LOUVER SCHEDULE													
MADIZ	MADIC OFM TYPE		MATERIAL			OPENING SIZE	DELTAD	MANUFACUTRER	DEMARKO					
MARK	CFM	TYPE	MATERIAL	WIDTH(IN)	WIDTH(IN) HEIGHT(IN) VELOCITY (FPM) FREE		FREE AREA (SF)	DELTA P	AND MODEL NUMBER	REMARKS				
L1	310	EXHAUST	ALUMINIUM	12.0	18.0	600	0.50	0.1	POTTORFF EFD-445	1,2,3,4,5				
L2	550	INTAKE	ALUMINIUM	12.0	30.0	600	0.92	0.1	POTTORFF EFD-445	1,2,3,4,5				
L3	1,500	INTAKE	ALUMINIUM	24.0	36.0	600	2.50	0.1	POTTORFF EFD-445	1,2,3,4,5				
L4	830	EXHUAST	ALUMINIUM	18.0	30.0	600	1.37	0.1	POTTORFF EFD-445	1,2,3,4,5				
L5	770	EXHUAST	ALUMINIUM	18.0	30.0	600	1.30	0.1	POTTORFF EFD-445	1,2,3,4,5				

OR APPROVED EQUAL

2. PROVIDE EXTRUDED ALUMINUM, 4" DRAINABLE STATIONARY WALL LOUVER WITH BIRD SCREEN.

3. PROVIDE LOUVER WITH ANODIZED FINISH, COORDINATE COLOR WITH ARCHITECT

4. PROVIDE WITH EXTENDED SILL.

5. PROVIDE TRANSITION OR ADAPTOR WHERE REQUIRED TO ADAPT DUCTWORK TO NECK SIZE.

	AIR DEVICE SCHEDULE													
MARK	SERVES	NECK SIZE (INCHES)	FACE SIZE (INCHES)	MOUNTING	ТҮРЕ	MATERIAL	MAXIMUM NC	DESIGN BASIS MANUFACTURER/ MODEL SERIES	REMARKS					
S1	SUPPLY	8	48 x 4	CEILING	SLOT	ALUMINUM	25	TITUS/ML-37	16					
S2	SUPPLY	6,8,10	24 x 24	CEILING	LOUVERED	ALUMINUM	25	TITUS/TDCA	1,2					
S3	SUPPLY	6,8	24 x 24	CEILING	LOUVERED	ALUMINUM	25	TITUS/OMNI	1,2					
R1	RETURN	8	48 x 4	CEILING	SLOT	STEEL	30	TITUS/MLR-37	1,2,3,6					
R2	RETURN	6,8,10	24 x 24	CEILING	LOUVERED	STEEL	30	TITUS/PAR	1,2					
E1	EXHAUST	6,8,10,12,14	24 x 24	CEILING	LOUVERED	STEEL	30	TITUS/PAR	1,2					
E2	EXHAUST	6	12 x 12	CEILING	LOUVERED	STEEL	30	TITUS/PAR	1,2					

REMARKS:

1. PROVIDE MOUNTING FRAME TO BE COMPATIBLE WITH TYPE OF CEILING IN WHICH THE DEVICE IS TO BE MOUNTED.

REFER TO ARCHITECTURAL REFLECTED CEILING PLAN FOR CEILING TYPES.

2. WHERE ROUND NECK SIZE IS NOTED ON DUCTWORK PLAN, PROVIDE RECTANGULAR TO ROUND DUCT COLLAR.

3. PROVIDE WITH ONE (1) 1/2" SLOTS.

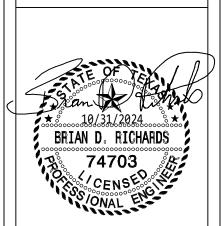
4. PROVIDE WITH BORDER 2A.

5. PROVIDE WITH MPI INSULATED PLENUM. 6. SLOT BORDER IS X-X, CONTRACTOR TO COORDINATE. **ENGINEERING UNLIMITED, INC.** 1300 Summit Avenue, Suite 514

Fort Worth, Texas 76102 Tel 817-529-6800 www.solare-eng.com Texas Registration # F-10963

PROJECT NO. : DATE : DRAWN: REVISED:

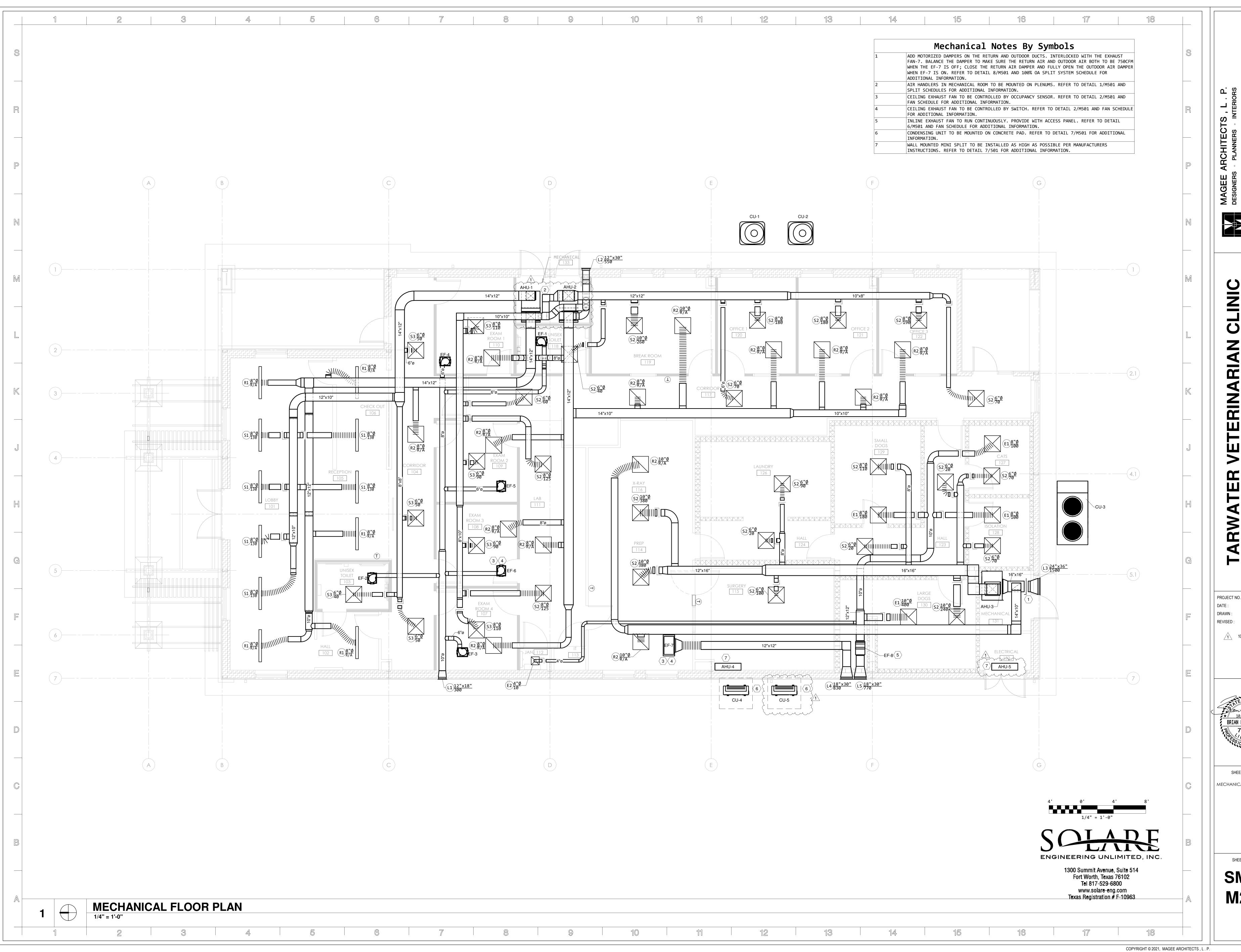
<u>/1</u> 10/31/2024



SHEET CONTENT MECHANICAL SCHEDULES

> SHEET NUMBER **SM01**

COPYRIGHT © 2021, MAGEE ARCHITECTS, L.P.



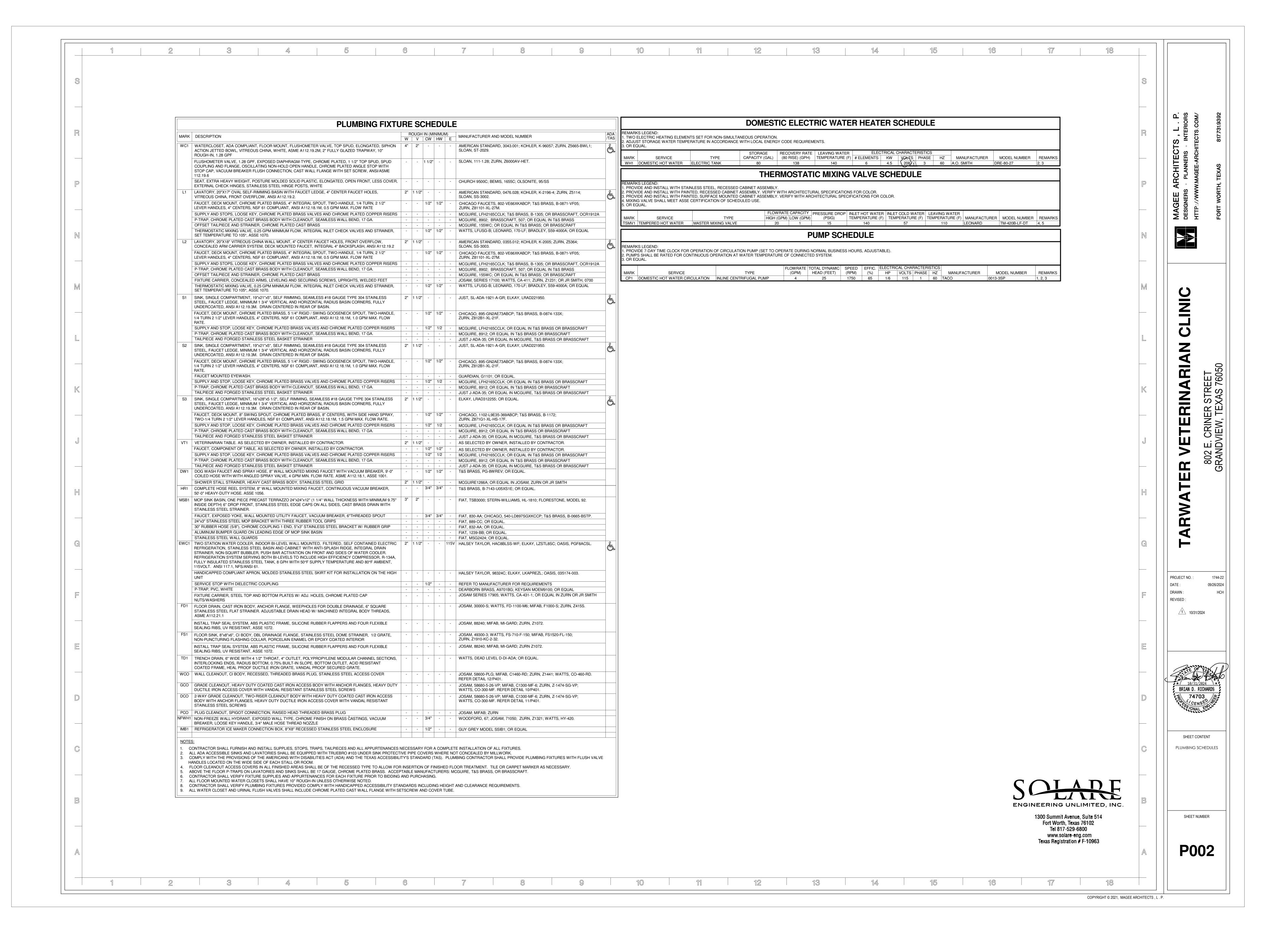
10/31/2024

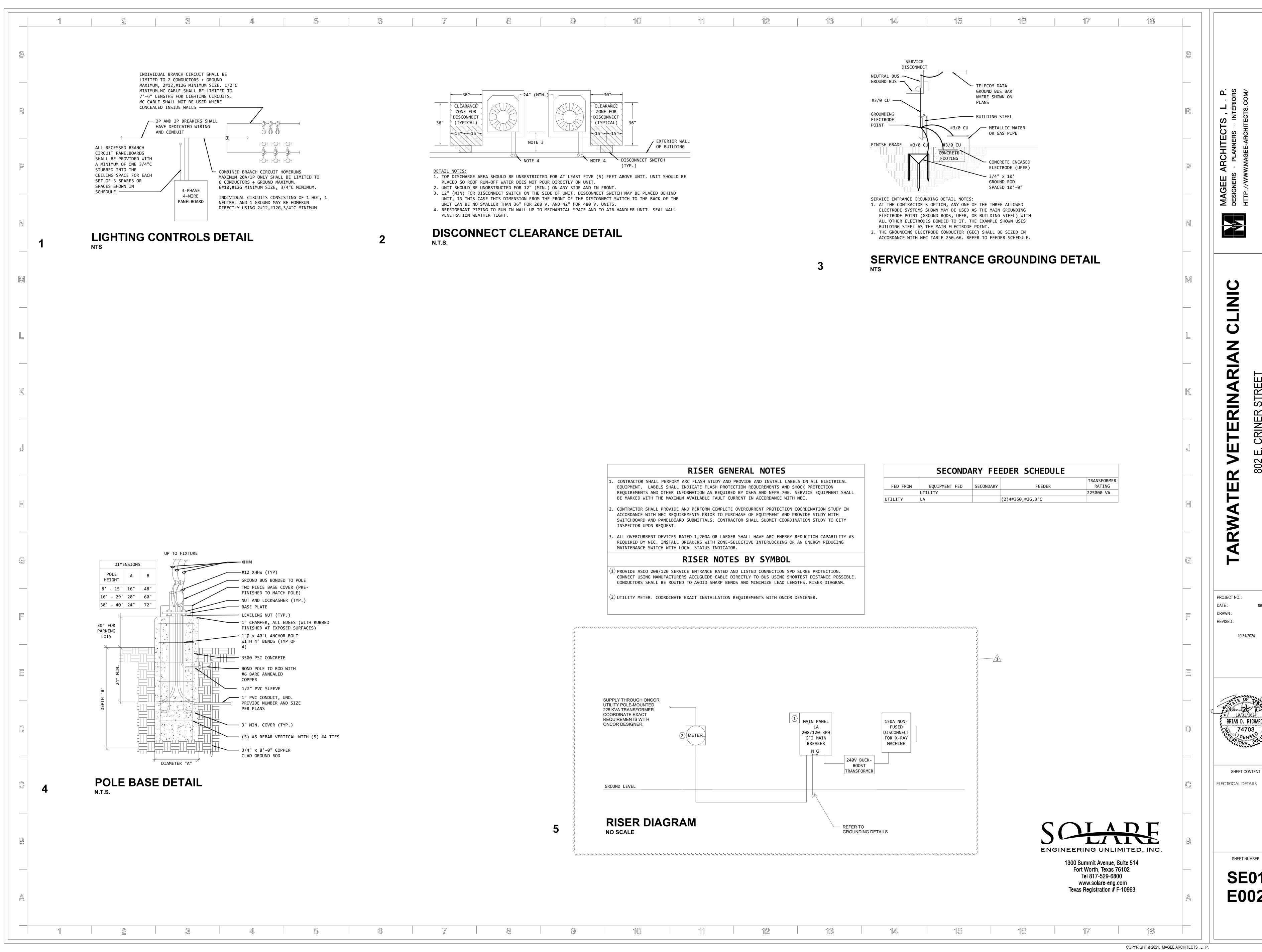
SHEET CONTENT

MECHANICAL FLOOR PLAN

SHEET NUMBER

SM02 M201

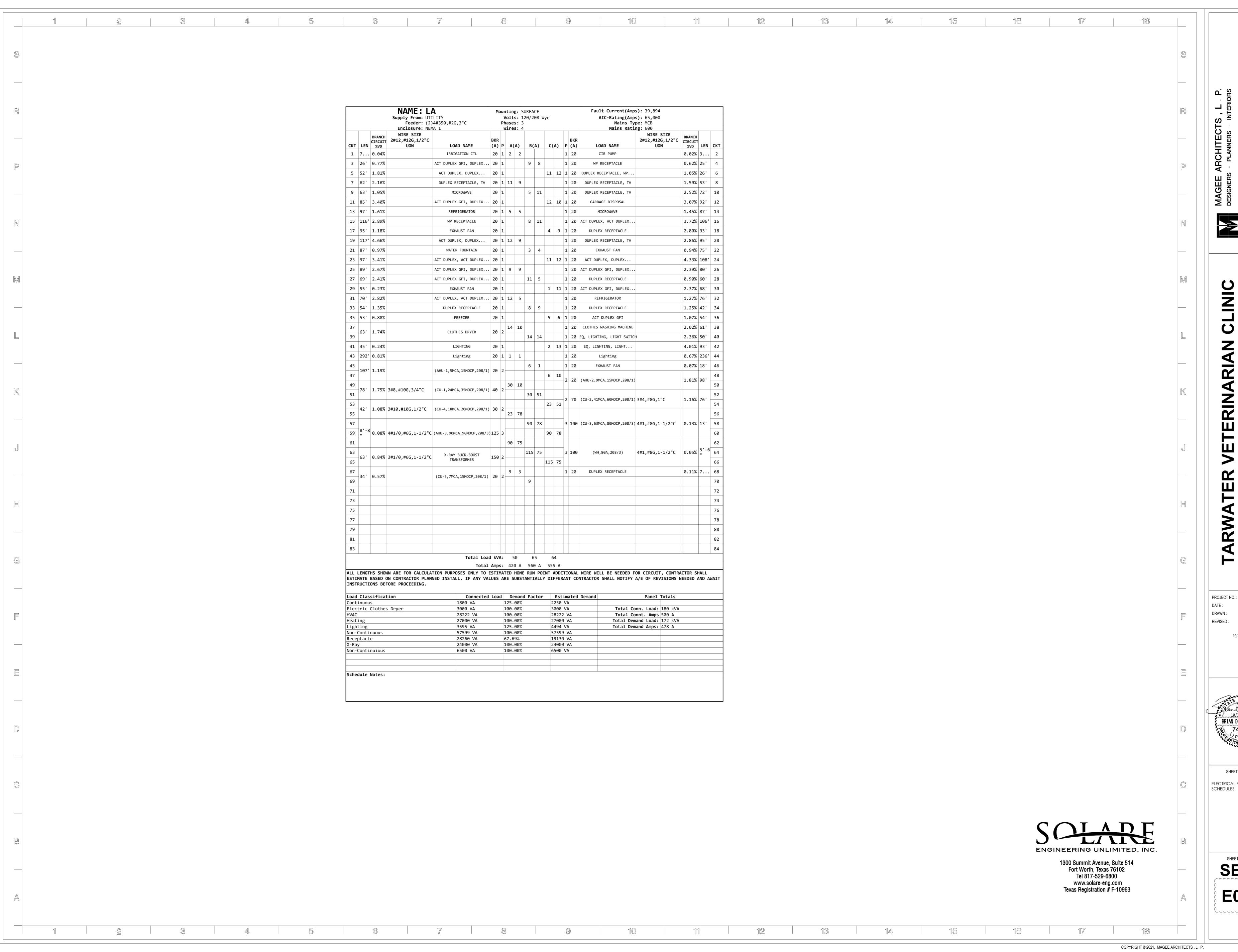




802 E. CRINER STF GRANDVIEW, TEXAS

10/31/2024

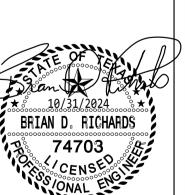
SHEET NUMBER **SE01 E002**



802 E. CRINE GRANDVIEW, ⁷

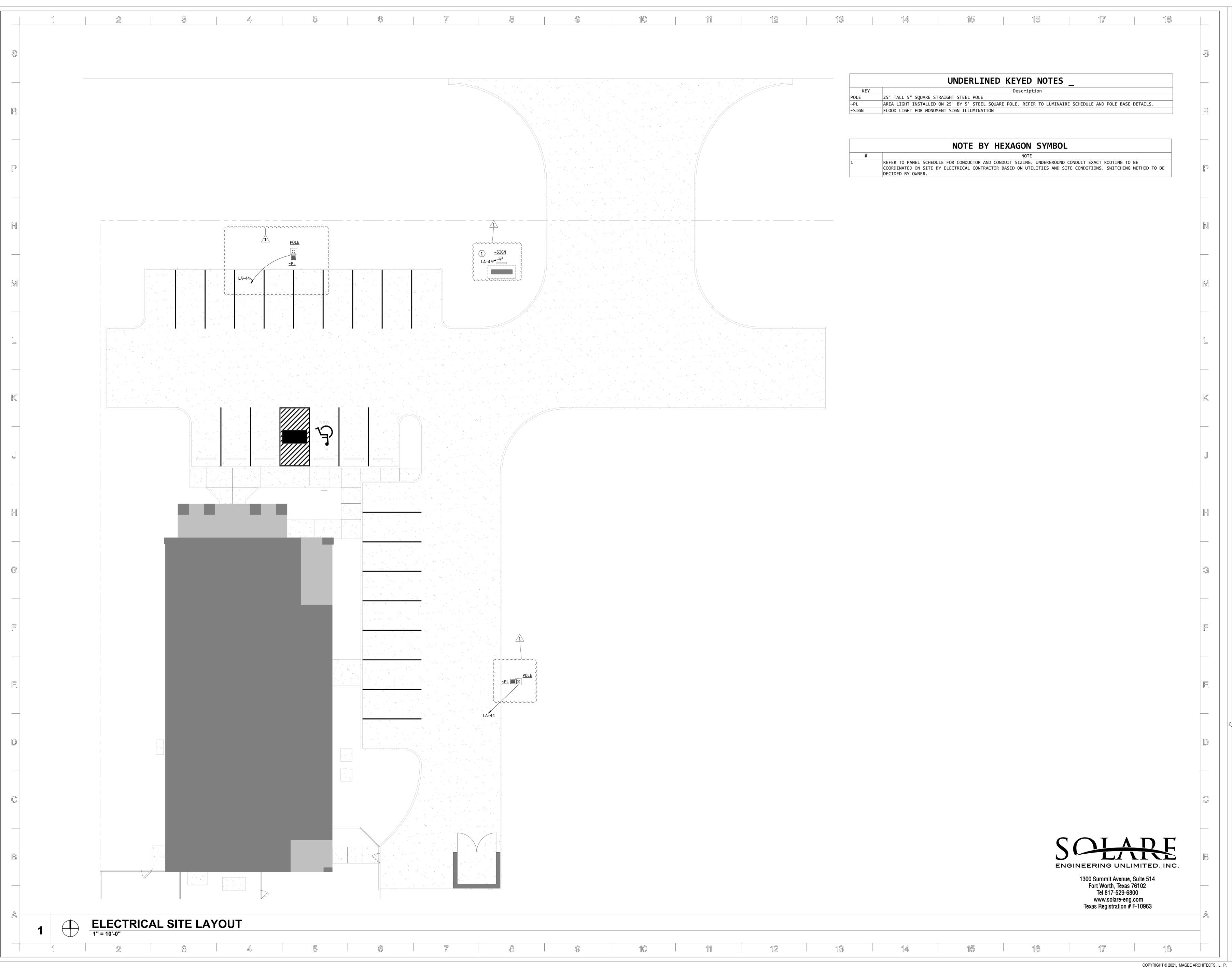
PROJECT NO.: DATE : DRAWN: REVISED:

10/31/2024



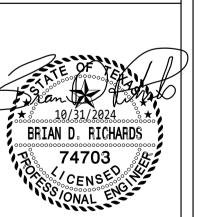
SHEET CONTENT ELECTRICAL PANELS

SHEET NUMBER **SE02 E003**



PROJECT NO.

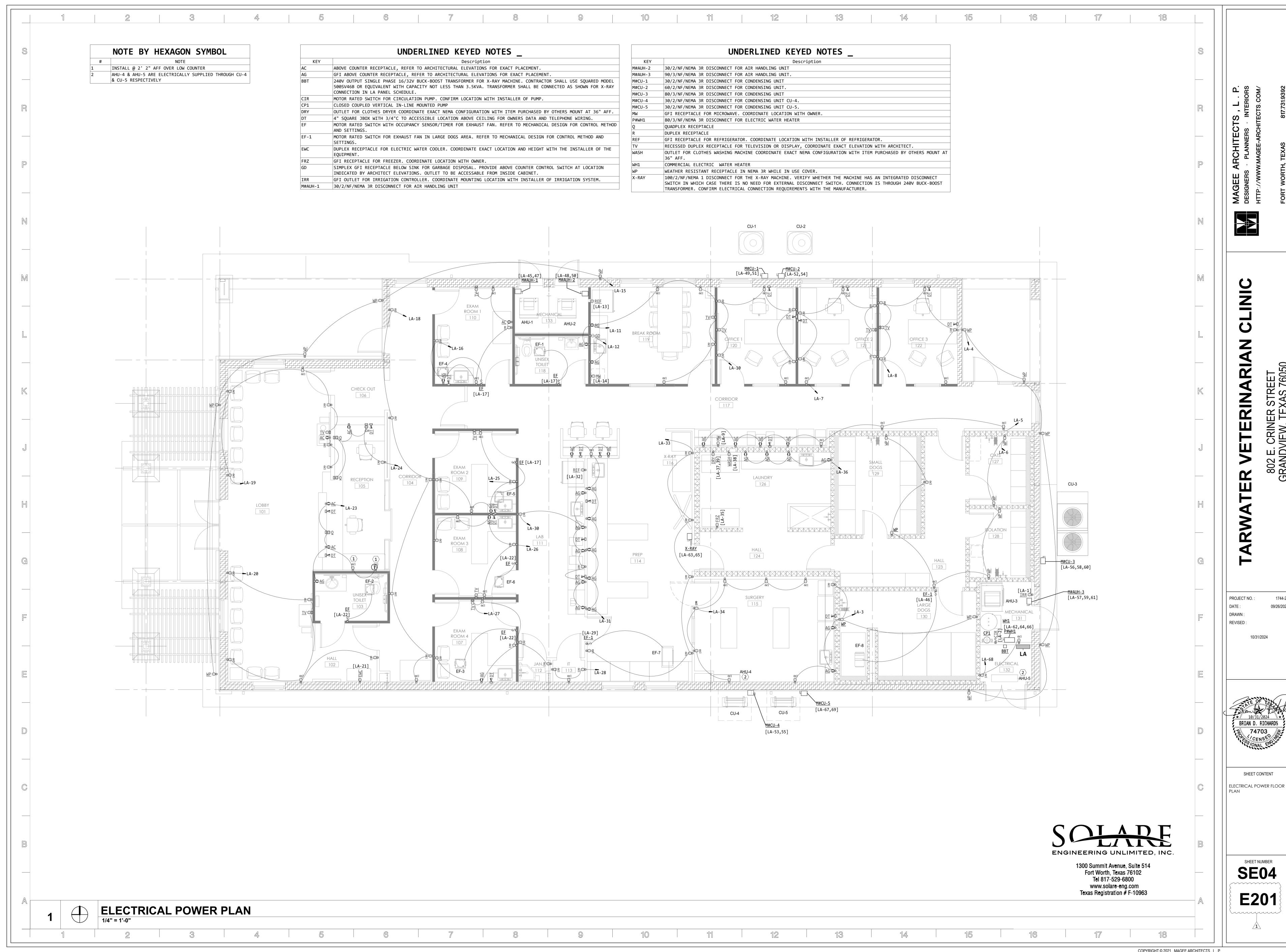
10/31/2024



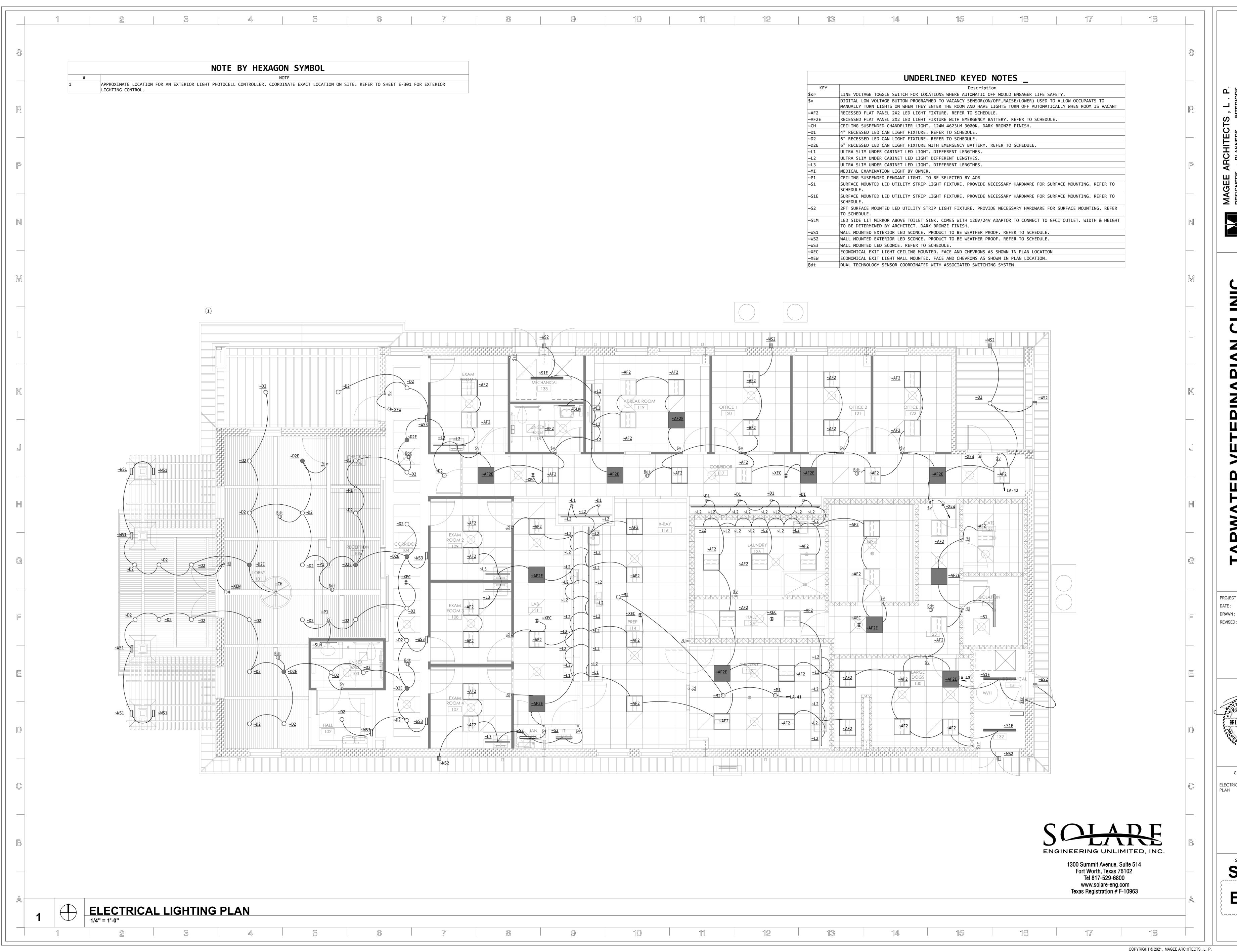
SHEET CONTENT ELECTRICAL SITE LAYOUT

SHEET NUMBER

SE03 E200



COPYRIGHT © 2021, MAGEE ARCHITECTS, L.P.



PROJECT NO.:

10/31/2024

SHEET CONTENT

ELECTRICAL LIGHTING FLOOR PLAN

SHEET NUMBER **SE05 E202**

mmmm